

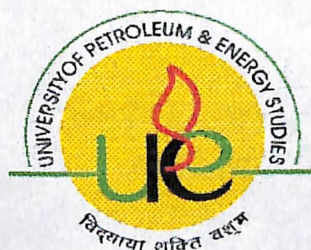
PERFORMANCE PREDICTION OF WATER-FLOODING SYSTEM USING ECLIPSE SIMULATOR

**DISSERTATION SUBMITTED
IN PARTIAL FULFILLMENT OF THE REQUIREMENT
FOR THE AWARD OF THE DEGREE OF
BACHELOR OF TECHNOLOGY
IN
PETROLEUM ENGINEERING**

BY:

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**UNDER THE GUIDANCE OF
Prof: Dr B.P.Pandey**



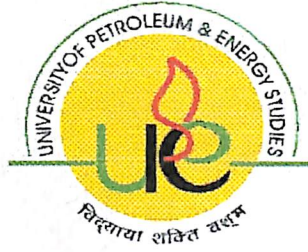
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CERTIFICATE

This is to certify that this dissertation, entitled “PERFORMANCE PREDICTION OF WATER FLOOD-SYSTEM USING ECLIPSE SIMULATOR” is a record of project carried out by Sidharth Sattiraju (R010103039), T.Ashwini Kumar (R010103044), and is submitted towards partial fulfillment of the requirements for the award of the degree of B.Tech in Applied Petroleum Engineering, University Of Petroleum & Energy Studies, Dehradun.

The content of this dissertation has not been a basis for any previous degree to him, or to the best of my knowledge, to any other person.

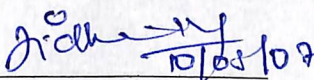
(Prof: Dr. B P Pandey)

ACKNOWLEDGEMENT

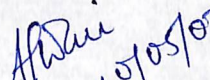
There are many who have helped us, in one way or another, in the completion of this project, and to whom thanks are due. In particular, we would like to place our sincere thanks to Prof: Dr.B.P.Pandey for his invaluable help and advice in the preparation of this project. We would also like to extend our gratitude to our course coordinator Prof. C.K.Jain and Prof: Dr. Choubey for their support and help through out the preparation of this project.

We have made significant use of the wealth of petroleum literature available in the public domain. I apologize to particular author(s) if we failed to acknowledge the appropriate reference at the end of this project. Undoubtedly, this project contains slight errors that our countless hours of review did not uncover. We will appreciate notification by any domain specific member of errors in the text.

Above all else, we hope that this project proves beneficial to the rising petroleum engineers who may use it in their professional work.


10/05/07

(Sidharth Sattiraju)


10/05/07

(T. Ashwini Kumar)

ABSTRACT

To make an economic evaluation of a proposed water-flood project, it is necessary to predict the water flood performance, that is, to make a projection of oil productions, or recovery, for the anticipated life of the project. Performance prediction includes composite value of injection rate, producing rate, producing WOR, oil recovery and cumulative injected water, all versus time.

A variety of water-flood performance prediction methods are available today. They are essentially based on some kind of models, which simulate the mechanism of water flooding the reservoir with the help of one or more formational variables, like permeability heterogeneity, injection rate, displacement mechanism etc.

Displacement models simulate the displacement mechanism of waterflooding where an immiscible oil-water front drives the oil out of the reservoir and hence also known as "frontal displacement" provides the concept of overall floodability.

Buckley-Leverett were the first to model it for a linear system by propounding the theory of "Frontal advance equation" and it acted as a strong foundation from which a fundamental understanding of the displacement mechanism evolved.

This project uses a black oil eclipse simulator to study the various parameters involved in the water flooding. The raw data given by the simulator was used to construct charts showing ultimate recovery, percentage recovery as well as the various key parameters.

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1. WATERFLOODING PRACTICE

1.1. FACTORS TO CONSIDER IN WATERFLOODING

Thomas, Mahoney, and Winter (1989) pointed out that in determining the suitability of a candidate reservoir for waterflooding, the following reservoir characteristics must be considered:

- Reservoir geometry
- Fluid properties
- Reservoir depth
- Lithology and rock properties
- Fluid saturations
- Reservoir uniformity and pay continuity
- Primary reservoir driving mechanisms

Each of these topics is discussed in detail in the following subsections.

Reservoir Geometry

The areal geometry of the reservoir will influence the location of wells and, if offshore, will influence the location and number of platforms required. The reservoir's geometry will essentially dictate the methods by which a reservoir can be produced through water-injection practices.

An analysis of reservoir geometry and past reservoir performance is often important when defining the presence and strength of a natural water drive and, thus, when defining the need to supplement the natural injection. If a water-drive reservoir is classified as an active water drive, injection may be unnecessary.

Fluid Properties

The physical properties of the reservoir fluids have pronounced effects on the suitability of a given reservoir for further development by waterflooding. The viscosity of the crude oil is considered the most important fluid property that affects the degree of success of a waterflooding project. The oil viscosity has the important effect of determining the mobility ratio that, in turn, controls the sweep efficiency.

Reservoir Depth

Reservoir depth has an important influence on both the technical and economic aspects of a secondary or tertiary recovery project. Maximum injection pressure will increase with depth. The costs of lifting oil from very deep wells will limit the maximum economic water-oil ratios that can be tolerated, thereby reducing the ultimate recovery factor and increasing the total project operating costs. On the other hand, a shallow reservoir imposes a restraint on the injection pressure that can be used, because this must be less than fracture pressure. In waterflood operations, there is a critical pressure (approximately 1 psi/ft of depth) that, if exceeded, permits the injecting water to expand openings along fractures or to create fractures. This results in the channeling of the injected water or the bypassing of large portions of the reservoir matrix. Consequently, an

operational pressure gradient of 0.75 psi/ft of depth normally is allowed to provide a sufficient margin of safety to prevent pressure parting.

Lithology and Rock Properties

Thomas et al. (1989) pointed out that lithology has a profound influence on the efficiency of water injection in a particular reservoir. Reservoir lithology and rock properties that affect flood ability and success are:

- Porosity
- Permeability
- Clay content
- Net thickness

In some complex reservoir systems, only a small portion of the total porosity, such as fracture porosity, will have sufficient permeability to be effective in water-injection operations. In these cases, a water-injection program will have only a minor impact on the matrix porosity, which might be crystalline, granular, or vugular in nature. Although evidence suggests that the clay minerals present in some sands may clog the pores by swelling and deflocculating when waterflooding is used, no exact data are available as to the extent to which this may occur.

Tight (low-permeability) reservoirs or reservoirs with thin net thickness possess water-injection problems in terms of the desired water injection rate or pressure⁴. Note that the water-injection rate and pressure are roughly related by the following expression:

$$P_{inj} \propto \frac{i_w}{hk}$$

where

p_{inj} = water-injection pressure

i_w = water-injection rate

h = net thickness

k = absolute permeability

The above relationship suggests that to deliver a desired daily injection rate of i_w in a tight or thin reservoir, the required injection pressure might exceed the formation fracture pressure

Fluid Saturations

In determining the suitability of a reservoir for waterflooding, a high oil saturation that provides a sufficient supply of recoverable oil is the primary criterion for successful flooding operations. Note that higher oil saturation at the beginning of flood operations increases the oil mobility that, in turn, gives higher recovery efficiency.

Reservoir Uniformity and Pay Continuity

Substantial reservoir uniformity is one of the major physical criteria for successful waterflooding. For example, if the formation contains a stratum of limited thickness with a very high permeability (i.e., thief zone), rapid channeling and bypassing will develop.

Unless this zone can be located and shut off, the producing water–oil ratios will soon become too high for the flooding operation to be considered profitable.

The lower depletion pressure that may exist in the highly permeable zones will also aggravate the water-channeling tendency due to the high permeability variations. Moreover, these thief zones will contain less residual oil than the other layers, and their flooding will lead to relatively lower oil recoveries than other layers.

Areal continuity of the pay zone is also a prerequisite for a successful waterflooding project. Isolated lenses may be effectively depleted by a single well completion, but a flood mechanism requires that both the injector and producer be present in the lens. Breaks in pay continuity and reservoir anisotropy caused by depositional conditions, fractures, or faulting need to be identified and described before determining the proper well spanning and the suitable flood pattern orientation.

1.2. OPTIMUM TIME TO WATERFLOOD

The most common procedure for determining the optimum time² to start waterflooding is to calculate:

- Anticipated oil recovery
- Fluid production rates
- Monetary investment
- Availability and quality of the water supply
- Costs of water treatment and pumping equipment
- Costs of maintenance and operation of the water installation facilities
- Costs of drilling new injection wells or converting existing production wells into injectors

These calculations should be performed for several assumed times and the net income for each case determined. The scenario that maximizes the profit and perhaps meets the operator's desirable goal is selected.

Cole (1969) lists the following factors as being important when determining the reservoir pressure (or time) to initiate a secondary recovery project:

Reservoir oil viscosity

Water injection should be initiated when the reservoir pressure reaches its bubble-point pressure since the oil viscosity reaches its minimum value at this pressure. The mobility of the oil will increase with decreasing oil viscosity, which in turns improves the sweeping efficiency.

Free gas saturation

(1) In water injection projects. It is desirable to have initial gas saturation, possibly as much as 10%. This will occur at a pressure that is below the bubble point pressure. (2) In

gas injection projects. Zero gas saturation in the oil zone is desired. This occurs while reservoir pressure is at or above bubble-point pressure.

Cost of injection equipment

This is related to reservoir pressure, and at higher pressures, the cost of injection equipment increases. Therefore, a low reservoir pressure at initiation of injection is desirable.

Productivity of producing wells

A high reservoir pressure is desirable to increase the productivity of producing wells, which prolongs the flowing period of the wells, decreases lifting costs, and may shorten the overall life of the project.

Effect of delaying investment on the time value of money

A delayed investment in injection facilities is desirable from this standpoint.

Overall life of the reservoir

Because operating expenses are an important part of total costs, the fluid injection process should be started as early as possible.

Some of these six factors act in opposition to others. Thus the actual pressure at which a fluid injection project should be initiated will require optimization of the various factors in order to develop the most favorable overall economics.

The principal requirement for a successful fluid injection project is that sufficient oil must remain in the reservoir after primary operations have ceased to render economic the secondary recovery operations. This high residual oil saturation after primary recovery is essential not only because there must be a sufficient volume of oil left in the reservoir, but also because of relative permeability considerations. A high oil relative permeability, i.e., high oil saturation, means more oil recovery with less production of the displacing fluid. On the other hand, low oil saturation means a low oil relative permeability with more production of the displacing fluid at a given time.

1.3. STAGES OF WATERFLOODING

There are 4 stages in waterflooding:

1. Start—interference
2. Interference—fill-up
3. Fill-up—water breakthrough
4. Water breakthrough—end of the project

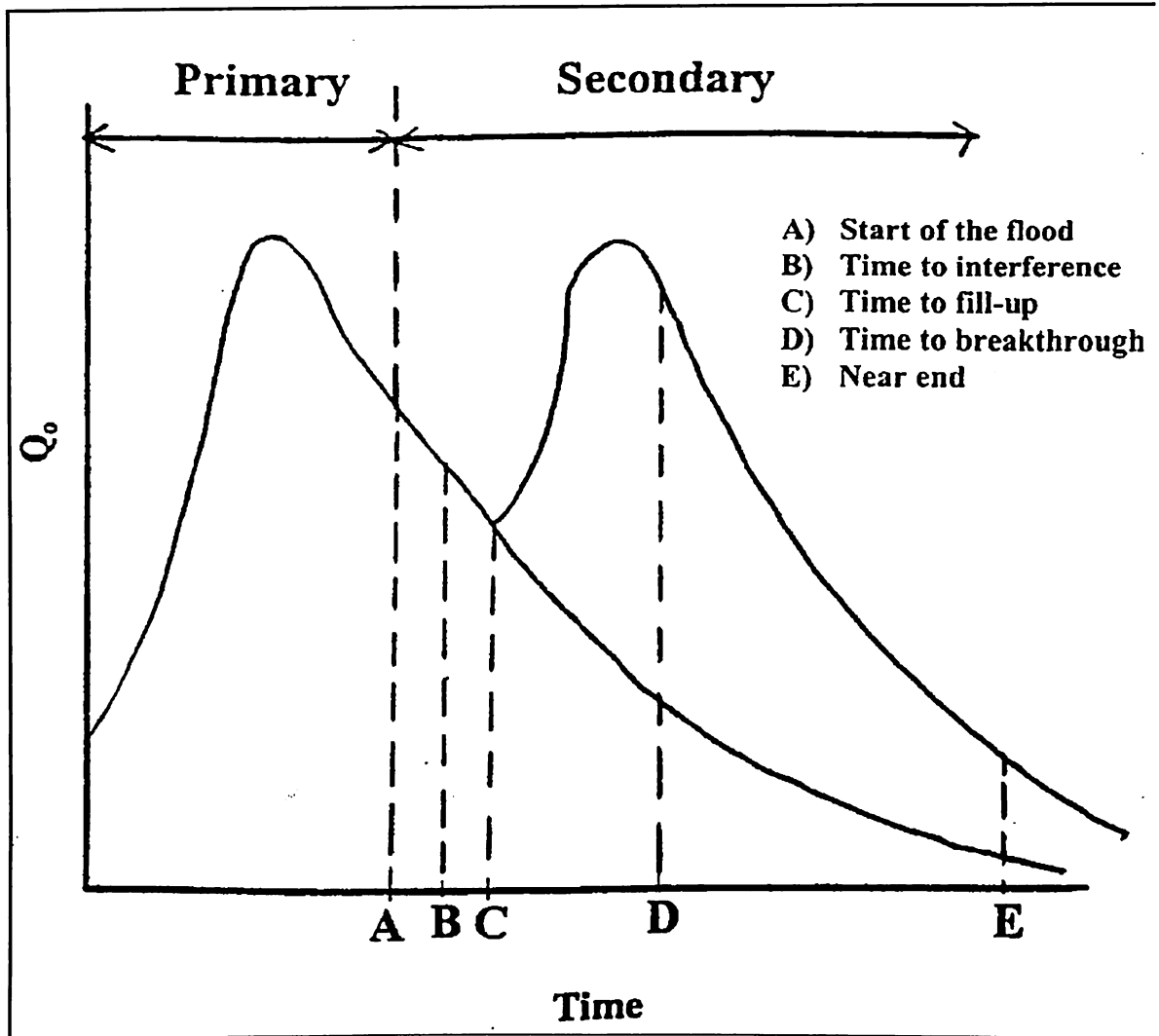


Figure 1. Predicted Production history

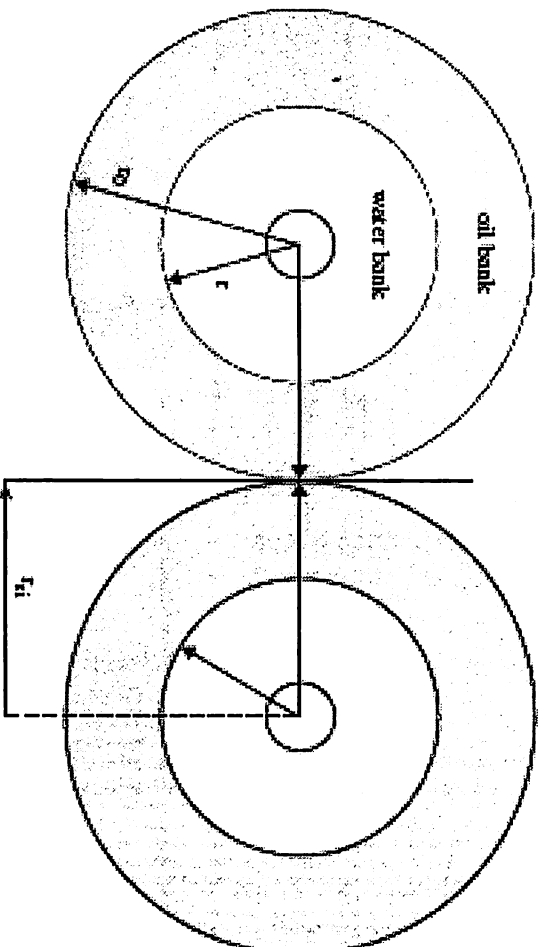


Figure 2. Interference of Oil banks

Stage 1: Start—Interference

At the start of the water-injection process in the selected pattern area of a solution-gas-drive reservoir, high gas saturation usually exists in the flood area as shown schematically in Figure 10.

The current oil production at the start of the flood is represented by point A on the conventional flow rate–time curve⁵ of Figure 10.

After the injection is initiated and a certain amount of water injected, an area of high water saturation called the water bank is formed around the injection well at the start of the flood. This stage of the injection is characterized by a radial flow system for both the displacing water and displaced oil.

With continuous water injection, the water bank grows radially and displaces the oil phase that forms a region of high oil saturation that forms an oil bank. This radial flow continues until the oil banks, formed around adjacent injectors, meet. The place where adjacent oil banks meet is termed Interference. During this stage of the flood, the condition around the producer is similar to that of the beginning of the flood, i.e., no changes are seen in the well flow rate Q_o .

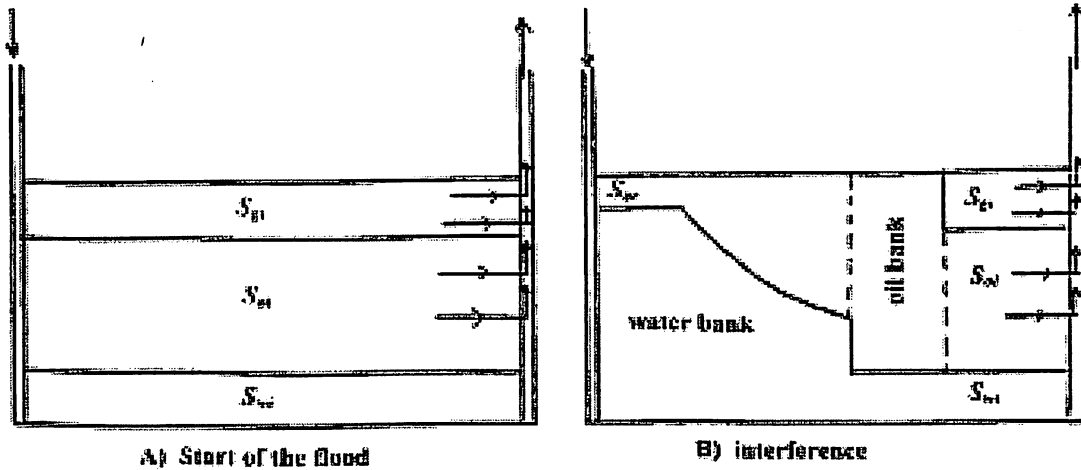


Figure 3. Start of Waterflood

Stage 2: Interference—Fill-Up

This stage describes the period from interference until the fill-up of the preexisting gas space. Fill-up is the start of oil production response as illustrated by point C on Figure 10. The flow during this time is not strictly radial and is generally complex to quantify mathematically. Therefore, the flood performance can only be determined at the time of fill-up.

Stage 3: Fill-up—Water Breakthrough

The time to fill-up, as represented by point C on Figure-10, marks the following four events:

1. No free gas remaining in the flood pattern
2. Arrival of the oil-bank front to the production well
3. Flood pattern response to the waterflooding
4. Oil flow rate Q_o equal to the water injection rate i_w

During this stage, the oil production rate is essentially equal to the injection due to the fact that no free gas exists in the swept flood area. With continuous water injection, the leading edge of the water bank eventually reaches the production well, as shown in Figure-13, and marks the time to breakthrough. At breakthrough the water production rises rapidly.

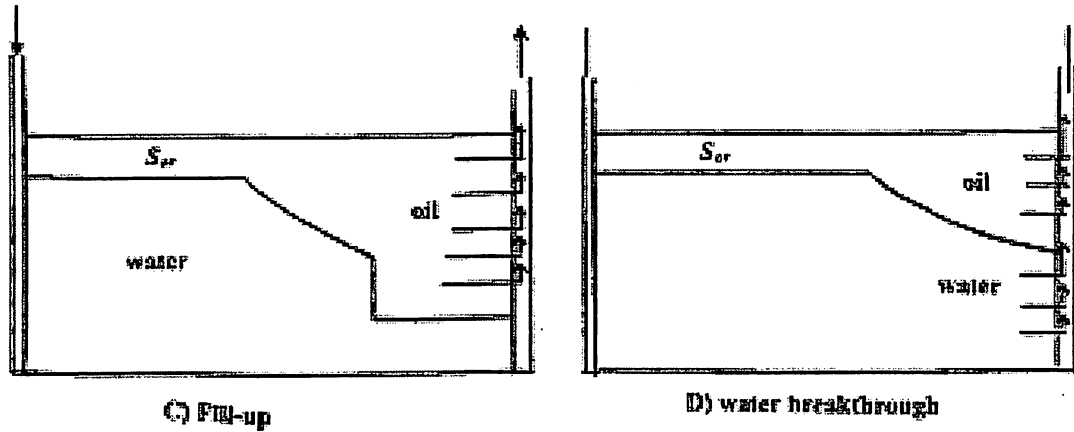
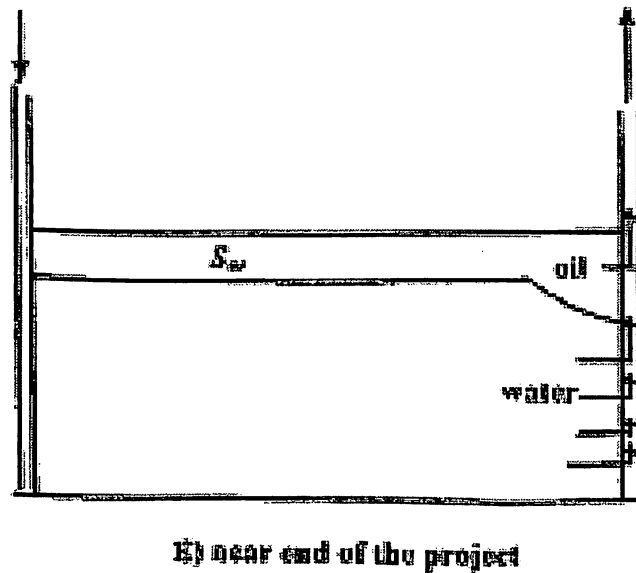


Figure4. Fill – up & Water breakthrough

Stage 4: Water Breakthrough—End of the Project

After breakthrough, the water–oil ratio increases rapidly with a noticeable decline in the oil flow rate as shown in by point D. The swept area will continue to increase as additional water is injected. The incrementally swept area will contribute additional oil production, while the previously swept area will continue to produce both oil and water.

Figure5. End of Project



2. RESERVOIR SIMULATION PROCESS & SIMULATORS

2.1. RESERVOIR SIMULATION PROCESS

Reservoir simulation⁷ involves solving partial differential equations that describe fluid flow in porous media with numerical methods, such as finite difference method. Partial differential equations are discretized with respect to time and space. A linear equation solver is used to solve all the equations generated in the discretization process.

General reservoir simulation process involves following steps:

- Reservoir characterization
- Simulation
- Simulation validation
- Reservoir management

Reservoir characterization:

- Field mapping
- Production data analysis
- Petrophysical analysis
- Rock characterization
- Fluid characterization
- Volumetric analysis

Field mapping:

- Areal and vertical extent of producing formation
- Isopach maps of gross and net sand thickness
- Correlation of layers and other zones

Reservoir rock characterization:

- Areal variations of average permeability, including directional trends derived from geological interpretations
- Areal variation of the porosity
- Reservoir heterogeneity particularly variation of permeability with thickness and zone

Fluid characterization:

- Relative permeability data for the reservoir rock, reservoir fluid properties include fluid viscosities, densities, FVF, gas solubilities etc. These data are usually obtained by laboratory tests.

Volumetric analysis and production data analysis:

- Included are the field performance histories, the production and injection histories, time dependent pressure distributions and well indexes, the production and injection histories include:
 1. WOR

2. GOR
 3. Oil, water & gas injection and production data
 4. Fluid break through times
 - a. Identification of producing mechanisms- such as fluid expansion, solution gas or water drives
 - b. Existence of gas caps or aquifers
 - c. Estimation of oil remaining to be produced under primary operations
 - d. Pressure distributions in the reservoir
 - e. Trapped gas saturation from solution gas drive
 - f. Vertical variation of saturation as a result of gravity segregation
 - g. Presence of mobile connate water
 - h. Areas already water flooded by natural water drive
- Reservoir simulation includes two steps:
 - a. Input file construction
 - b. History analysis

Input files construction:

- The necessary phase of every simulation study is the gathering of data to be used in the simulator.
- Values of the physical quantities must be specified before a simulation can begin.
- The particular data needed will depend on the nature and complexity of the study.
- Required data can be classified into 3 groups:
 1. Reservoir rock properties
 2. Fluid properties
 3. Field performance

History matching:

Objective of the history match⁶ is to reproduce with the simulator the actual reservoir performance. This is achieved by manipulating two fundamental processes that are controlled during history matching the quantity & distribution of fluid within the system. These processes are manipulated by adjusting input data within reasonable limits of conditions existing in the field until a minimal difference remains between the historical data and simulator calculations at same point in time.

Thus history matching is a process of determining poorly known and unknown physical parameters, which are needed as the input to the mathematical reservoir model. Much of the physically measurable information used in the simulator is based on the incomplete or inaccurate field measurements.

Prediction runs:

- After a satisfactory history match of field, performance is obtained within the simulator and prediction runs can be made.

- A number alternative field operations or development scenarios can be evaluated and compared in a short period of time to optimize future reservoir management planning for the field. Because there is no field history to use for comparison with the simulation result for prediction run, it is even more important that critical engineering judgement be applied to the results using the test of reasonabilities.
- Less accuracy in the simulation predictions should be expected when the prediction runs are simulating, operations under a different flow system than that of history matching process.
- A common example of this is history matching primary production performance and then matching predictions of performance under waterflood operations.
- The reason for this is that some uncertain reservoir parameters may have little effect on performance under flow in a gas oil system but may be of critical importance in water-oil system.
- This same caution applies in case of simulator predictions of EOR process performance. Obtaining the best possible reservoir description prior to the simulation work can minimize the potential problems.

Simulation validation:

- Perhaps the most pervasive source of error in the history matching process is the lack of reliable field data. There are many reasons why reported field data may be unreliable. Furthermost, the amount of data is usually limited. Thus the history match may characterize the reported data, but the reported data may not characterize the reservoir.
- Another source of error arises when the derivatives in the mathematical formulation of the model are placed by the finite differences. This error is called the truncation error called numerical dispersion. It can cause a correct set of parameters to yield incorrect results, such as predicting the premature water breakthrough.
- The uniqueness of the parameter sets, the inaccuracy or the incompleteness of the field data and presence of truncation errors in history matching. The engineer should be aware that these problems exist and can cause inexact performance projections.
- Accurate simulation results are dependent on having high quality data on a large number of reservoir parameters.
- One technique that is frequently used to help the guide the data gathering effort and to allocate the data collection time to the critical parameters is to use the simulation model to do sensitivity analysis on selected parameters. By varying each of several selected parameters over a reasonable range of uncertainty and obtaining the effect on simulator performance. The critical controlling parameters can be identified. Further efforts to gather data should be concentrated on these critical parameters.
- Some estimate of OOIP, either by volumetric or MBE, should be made before beginning any field wise simulation study. This independent OOIP calculation provides a check on the simulator input data and reservoir description.
- Also in a large study, the MBE calculation will provide a check on the consistency of the pressure, production and fluid PVT data. If these data cannot

give a reasonably consistent MBE calculation, then proceeding to an expensive simulator study is not justified.

2.2. ECLIPSE 100 SIMULATOR

ECLIPSE 100 is a fully-implicit, three phase, three dimensional, general purpose black oil simulator with gas condensate option. Program is written in FORTRAN77 and operate on any computer with an ANSI-standard FORTRAN77 compiler and with sufficient memory.

ECLIPSE 100 can be used to simulate 1, 2 or 3 phase systems. Two phase options (oil/water, oil/gas, gas/water) are solved as two component systems saving both computer storage and computer time. In addition to gas dissolving in oil (variable bubble point pressure or gas/oil ratio), ECLIPSE 100 may also be used to model oil vaporizing in gas (variable dew point pressure or oil/gas ratio).

Both corner-point and conventional block-center geometry options are available in ECLIPSE. Radial and Cartesian block-center options are available in 1, 2 or 3 dimensions. A 3D radial option completes the circle allowing flow to take place across the 0/360 degree interface.

3. PROBLEM FORMULATION

3.1. RESERVOIR DESCRIPTION

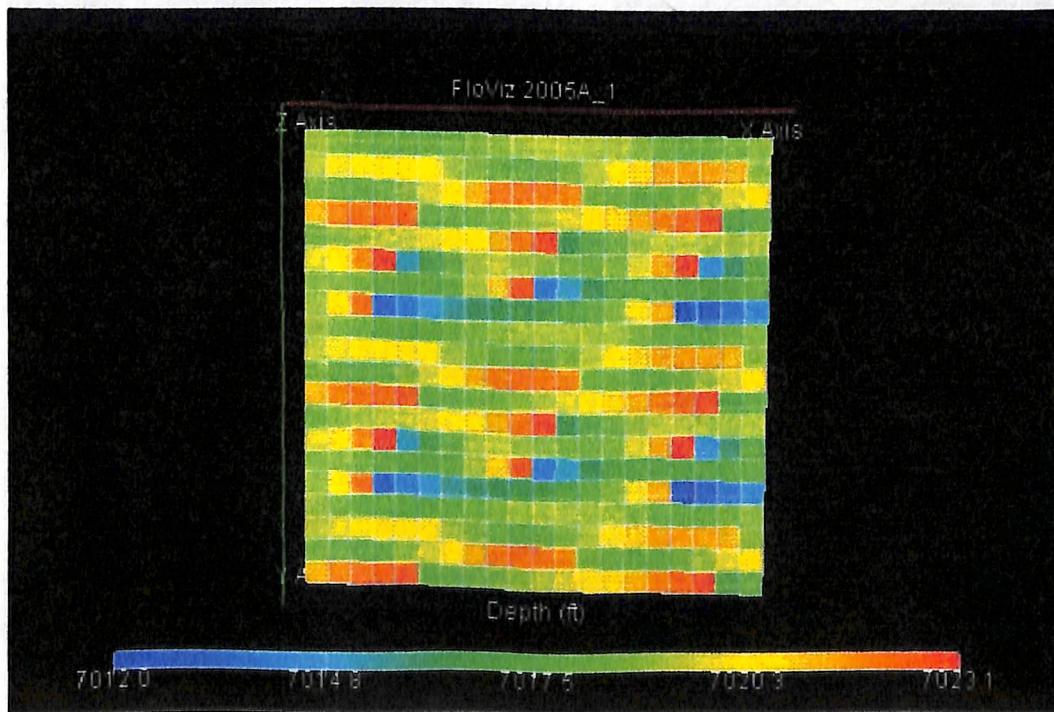
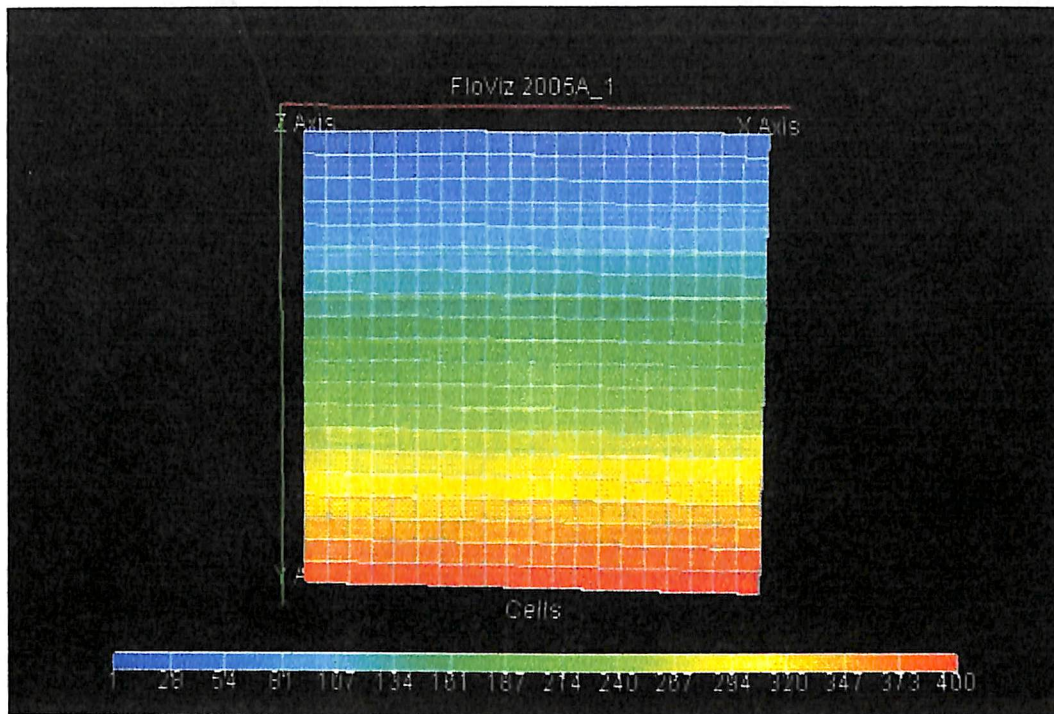
The reservoir to be studied is under production for 2 years. It is planned to waterflood the reservoir to get maximum recovery. This is to be simulated before implementing the plan to estimate the maximum recovery that can be achieved, and to experiment with various waterflood pattern and injection rates to be used.

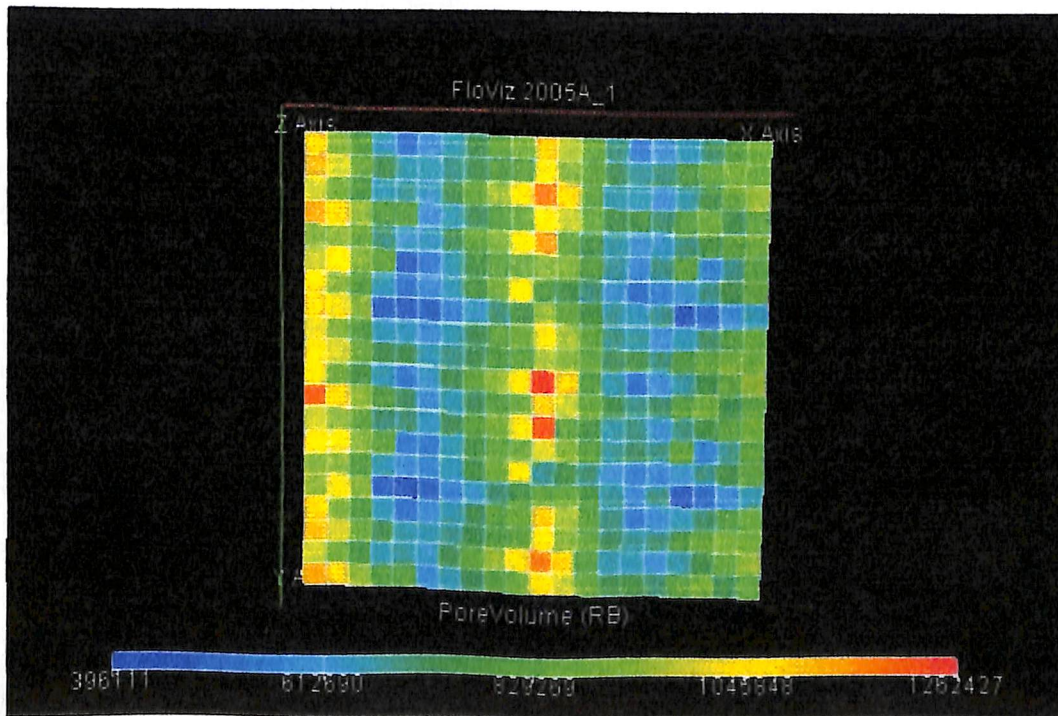
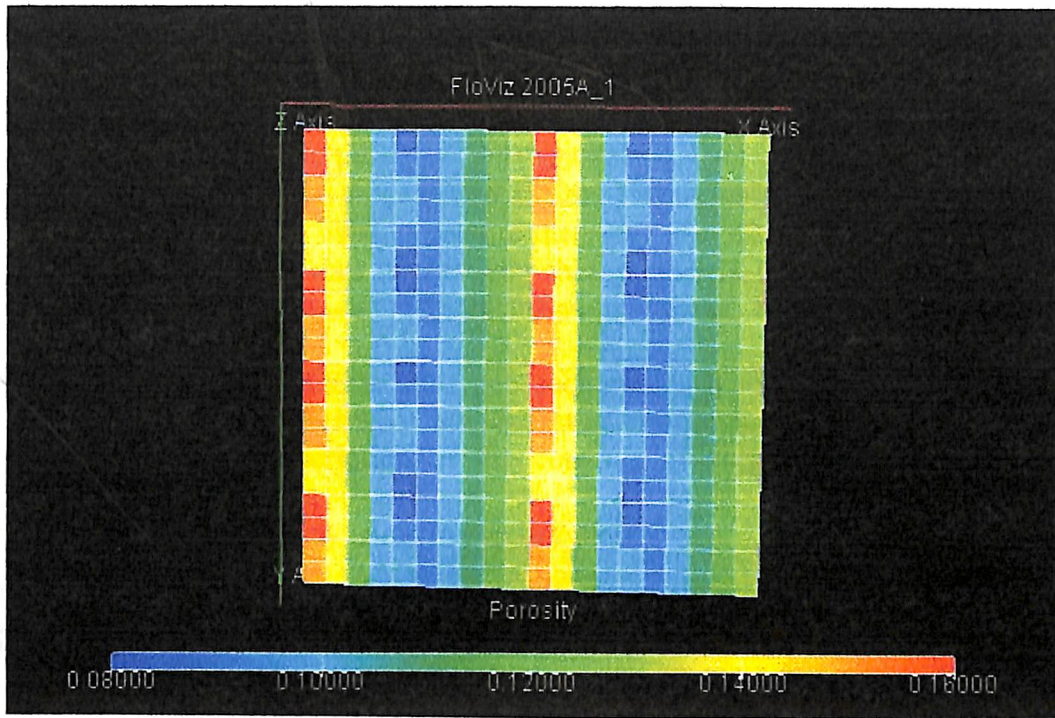
The area of the reservoir studied is 5.74 acres and pay thickness is completed in one layer. The net pay thickness is 20 feet. The reservoir is a homogeneous one and reservoir pressure is 6500 psi. The Oil Initially in Place is 45.38 MMstb. The porosity of the grid blocks are varying and are described in chapter 4. The permeability of the layer is varying throughout the grid blocks in x and y directions. The reservoir bubble point pressure is given by 1050 psi. The reservoir is producing under solution gas drive mechanism and contains 1 well. It was producing at a rate of 1500 bopd after 2 years.

Injection Rates

The reservoir is flooded with different injection rates by taking a fixed 5 spot pattern. The 4 injection wells are placed. Production rates are varied depending on the reservoir pressure. The well will be allowed to produce upto abandonment pressure. Injection pressure is kept constant.

3.2. RESERVOIR MODEL





4. PREDICTION RUNS

4.1. INPUT DATA FILE PREPARATION

- To run simulation you need an input file with all data concerning reservoir and process of its exploitation.
- Input data for ECLIPSE is prepared in free format using a keyword system. Any standard editor may be used to prepare the input file. Alternatively ECLIPSE Office may be used to prepare data interactively through panels, and submit runs.
- The name of input file has to be in the following format: *FILENAME.DATA*

An ECLIPSE data input file is split into sections, each of which is introduced by a section-header keyword. A list of all section-header keywords is given in following, together with a brief description of the contents of each section and examples of keywords using in file code.

The list of section-header keywords in proper order:

RUNSPEC

GRID

EDIT

PROPS

REGIONS

SOLUTION

SUMMARY

SCHEDULE

The sections must be specified in the shown order.

It is recommended that the body of sections which are not frequently changed be held in separate files which are included in the data using the INCLUDE keyword. A data record has to be ended with a slash [/]

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RUNSPEC (Status: Required)

Title, problem dimensions, switches, phases present, components etc.

GRID (Status: Required)

The GRID section determines the basic geometry of the simulation grid and various rock properties (porosity, absolute permeability, net-to-gross ratios) in each grid cell. From this information, the program calculates the grid block pore volumes, mid-point depths and inter-block transmissibilities.

EDIT (Status: Optional)

Modifications to calculated pore volumes, grid block centre depths and transmissibilities.

PROPS (Status: Required)

Tables of properties of reservoir rock and fluids as functions of fluid pressures, saturations and compositions (density, viscosity, relative permeability, capillary pressure etc.). Contains the equation of state description in compositional runs.

REGIONS (Status: Optional)

Splits computational grid into regions for calculation of:

- PVT properties (fluid densities and viscosities),
- saturation properties (relative permeabilities and capillary pressures)
- initial conditions, (equilibrium pressures and saturations)
- fluids in place (fluid in place and inter-region flows)

If this section is omitted, all grid blocks are put in region 1.

SOLUTION (Status: Required)

Specification of initial conditions in reservoir - may be:

- calculated using specified fluid contact depths to give potential equilibrium
- read from a restart file set up by an earlier run
- specified by the user for every grid block (not recommended for general use)

This section contains sufficient data to define the initial state (pressure, saturations, compositions) of every grid block in the reservoir.

SUMMARY (Status: Optional)

Specification of data is to be written to the Summary file after each time step. Necessary if certain types of graphical output (for example water-cut as a function of time) are to be generated after the run has finished. If this section is omitted no Summary files are created.

SCHEDULE (Status: Required)

Specifies the operations to be simulated (production and injection controls and constraints) and the times at which output reports are required. Vertical flow performance curves and simulator tuning parameters may also be specified in the SCHEDULE section.

4.2. INPUT DATA FILE

RUNSPEC

TITLE
INITIAL

DIMENS
20 20 1 /

OIL

WATER

FIELD

WELLDIMS
5 1 2 4/

START
1 'JAN' 2007 /

UNIFOUT

--

GRID

BOX
1 20 1 20 1 1 /

DXV
20*500 /

DYV
20*500 /

DZ
38.2 37.4 36.6 36.0 35.8 36.0 36.6 37.3 38.0 38.5 38.7 38.7
38.6 38.6 37.6 36.7 36.2 36.3 37.0 37.9
39.1 40.1 41.0 41.2 41.1 40.8 38.5 37.5 36.5 35.8 36.4 37.5
38.9 40.4 41.9 43.2 43.4 43.1 42.6 38.1
37.3 36.4 35.8 36.6 38.0 39.5 41.1 42.8 44.3 44.6 44.3 44.0
37.3 37.0 36.6 36.6 37.3 38.4 39.7 41.1
42.5 43.8 44.5 44.8 45.0 36.2 36.6 37.0 37.4 38.1 38.8 39.7
40.6 41.7 42.8 43.8 44.8 45.6 34.8 36.0
37.1 38.0 38.6 39.0 39.3 39.7 40.4 41.4 42.8 44.4 46.0 32.9
35.1 37.1 38.5 39.1 39.0 38.7 38.6 38.8
39.7 41.4 43.7 46.2 30.6 33.8 36.7 38.7 39.1 38.5 37.8 37.3
37.1 37.7 39.8 42.9 46.0 28.7 32.1 35.3
37.7 38.0 37.3 36.6 36.0 35.7 36.2 38.6 42.0 45.3 27.3 30.1
32.7 34.7 35.4 35.2 34.9 34.8 35.0 36.0
38.2 41.1 44.2 25.8 27.8 29.8 31.3 32.3 32.8 33.1 33.6 34.4
35.7 37.8 40.2 42.7 24.0 25.5 27.0 28.2
38.2 37.4 36.6 36.0 35.8 36.0 36.6 37.3 38.0 38.5 38.7 38.7
38.6 38.6 37.6 36.7 36.2 36.3 37.0 37.9

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39.1	40.1	41.0	41.2	41.1	40.8	38.5	37.5	36.5	35.8	36.4	37.5
38.9	40.4	41.9	43.2	43.4	43.1	42.6	38.1				
37.3	36.4	35.8	36.6	38.0	39.5	41.1	42.8	44.3	44.6	44.3	44.0
37.3	37.0	36.6	36.6	37.3	38.4	39.7	41.1				
42.5	43.8	44.5	44.8	45.0	36.2	36.6	37.0	37.4	38.1	38.8	39.7
40.6	41.7	42.8	43.8	44.8	45.6	34.8	36.0				
37.1	38.0	38.6	39.0	39.3	39.7	40.4	41.4	42.8	44.4	46.0	32.9
35.1	37.1	38.5	39.1	39.0	38.7	38.6	38.8				
39.7	41.4	43.7	46.2	30.6	33.8	36.7	38.7	39.1	38.5	37.8	37.3
37.1	37.7	39.8	42.9	46.0	28.7	32.1	35.3				
37.7	38.0	37.3	36.6	36.0	35.7	36.2	38.6	42.0	45.3	27.3	30.1
32.7	34.7	35.4	35.2	34.9	34.8	35.0	36.0				
38.2	41.1	44.2	25.8	27.8	29.8	31.3	32.3	32.8	33.1	33.6	34.4
35.7	37.8	40.2	42.7	24.0	25.5	27.0	28.2				
38.2	37.4	36.6	36.0	35.8	36.0	36.6	37.3	38.0	38.5	38.7	38.7
38.6	38.6	37.6	36.7	36.2	36.3	37.0	37.9				
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38.9	40.4	41.9	43.2	43.4	43.1	42.6	38.1				
37.3	36.4	35.8	36.6	38.0	39.5	41.1	42.8	44.3	44.6	44.3	44.0
37.3	37.0	36.6	36.6	37.3	38.4	39.7	41.1				
42.5	43.8	44.5	44.8	45.0	36.2	36.6	37.0	37.4	38.1	38.8	39.7
40.6	41.7	42.8	43.8	44.8	45.6	34.8	36.0				

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PORO

0.16	0.14	0.12	0.1	0.08	0.09	0.1	0.11	0.12	0.13	0.16	0.14	0.12	0.1	0.08
0.09	0.1	0.11	0.12	0.13										
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0.16	0.14	0.12	0.1	0.08	0.09	0.1	0.11	0.12	0.13	0.16	0.14	0.12	0.1	0.08
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0.15	0.14	0.12	0.1	0.10	0.09	0.1	0.11	0.12	0.13	0.15	0.14	0.12	0.1	0.10
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0.09	0.1	0.11	0.12	0.13										
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0.16	0.14	0.12	0.1	0.09	0.09	0.1	0.11	0.12	0.13	0.16	0.14	0.12	0.1	0.09
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0.15	0.14	0.12	0.1	0.10	0.09	0.1	0.11	0.12	0.13	0.15	0.14	0.12	0.1	0.10
0.09	0.1	0.11	0.12	0.13										
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0.09	0.1	0.11	0.12	0.13										

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PERMX

150 150 8*160 3*40 4*160 2*80 146
140 150 8*160 3*50 4*134 2*68 147
130 150 8*165 3*40 4*142 2*75 149
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PERMY

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50 150 8*175 3*130 4*150 2*80 146

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PERMZ

400*150 /

ENDBOX

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TOPS

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INIT

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EDIT

PROPS

SWOF

-- Sw	krw	kro	Pcwo
0.20	0.000000	0.900000	0
0.25	0.000364	0.709187	0
0.30	0.002536	0.544963	0
0.35	0.007892	0.405962	0
0.40	0.017660	0.290741	0
0.45	0.032987	0.197760	0
0.50	0.054960	0.125368	0
0.55	0.084625	0.071765	0
0.60	0.122991	0.034959	0
0.65	0.171041	0.012686	0
0.70	0.229732	0.002243	0
0.75	0.300000	0.000000	0

/

-- Specifies PVT properties of OIL

PVDO

400	1.012	1.16
1200	1.0040	1.164
2000	0.9960	1.167
2800	0.9880	1.172
3600	0.9802	1.177
4400	0.9724	1.181
5200	0.9646	1.185
5600	0.9607	1.19

/

PVTW

1050	1	2.67E-06	0.56341	1.20E-07 /
------	---	----------	---------	------------

RSCONST

0.37	1050	/
------	------	---

DENSITY

47	63.0200	/
----	---------	---

ROCK

1050.0	5.0E-06 /
--------	-----------

REGIONS

SOLUTION

EQUIL

7020	6500	7020	0	0	/
------	------	------	---	---	---

SUMMARY

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-- Average pressure for field.
FPR

-- Oil production total
FOPT

-- Water injection total of field
FWIT

--Water cut
FWCT

--OIL IN PLACE
FOIP

-- FORMATION WATER SATURATION
FWSAT

--Water Reservoir Volume in Place
FWIPR

--Fraction of total oil produced by water influx
FORFW

--FORM OIL PORE VOL
FOPV

--FORM WATER PORE VOL
FWPV

--OIL RECOVERY
FOE

--GOR
FGOR

--Water production
FWPT

-- Average pressure for field.
FPR

-- Oil production total
FOPT

-- Water injection total of field
FWIT

--Water production
FWPT

-- WATER GAS RATIO
FWGR

EXCEL

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SCHEDULE

WELSPECS

P G1 10 10 7015 'OIL' /
/

COMPDAT

P 10 10 1 1 'OPEN' 2* 0.2 /
/

WCONPROD

P 'OPEN' ORATE 1500 4* 1000/
/

TSTEP

31	28	31	30	31	30	31	31	30	31	30	31
31	28	31	30	31	30	31	31	30	31	30	31

/

WELSPECS

I1 G2 7 10 7015 'WAT' /
I2 G2 13 10 7015 'WAT' /
I3 G2 10 7 7015 'WAT' /
I4 G2 10 13 7015 'WAT' /
/

COMPDAT

I1 7 10 1 1 'OPEN' 2* 0.2 /
I2 13 10 1 1 'OPEN' 2* 0.2 /
I3 10 7 1 1 'OPEN' 2* 0.2 /
I4 10 13 1 1 'OPEN' 2* 0.2 /
/

WCONPROD

P 'OPEN' ORATE 1500 4* 1000/
/

WCONINJE

I1 WATER OPEN RATE 4000 1* 5000/
I2 WATER OPEN RATE 4000 1* 5000/
I3 WATER OPEN RATE 4000 1* 5000/
I4 WATER OPEN RATE 4000 1* 5000/
/

TSTEP

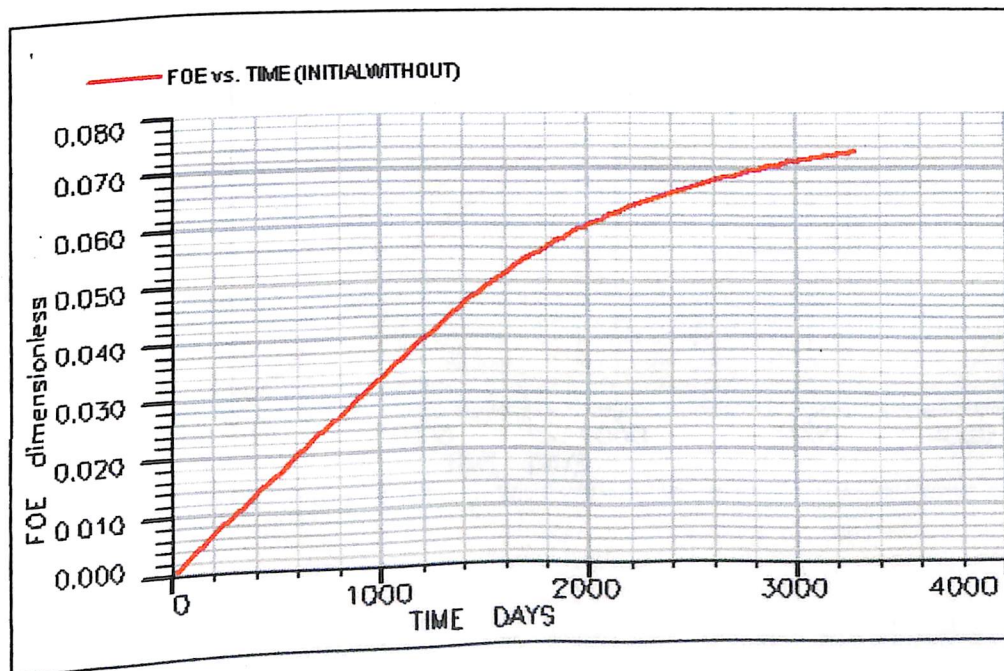
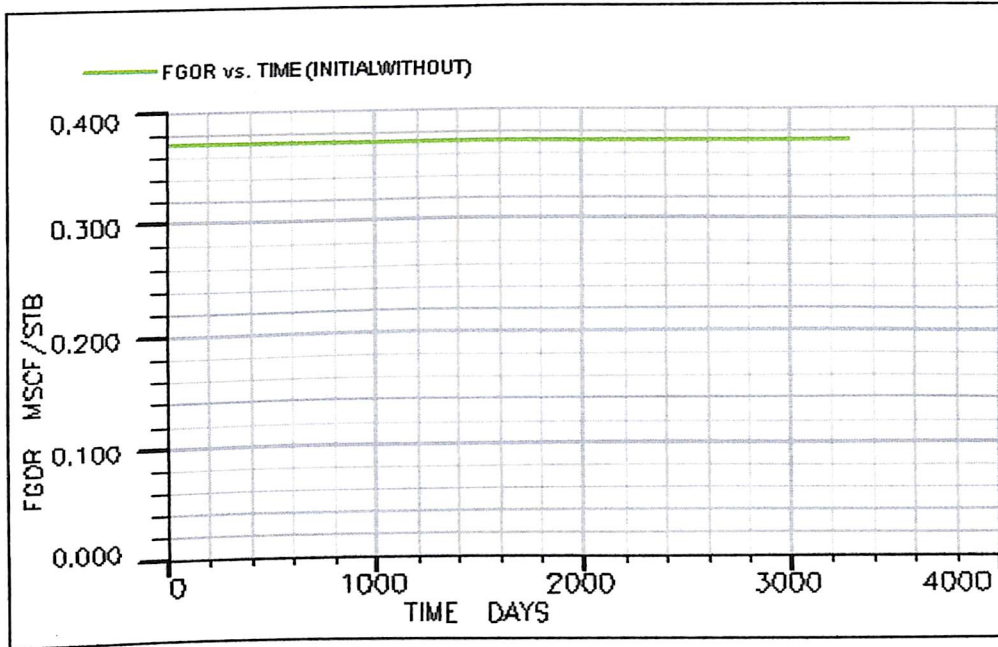
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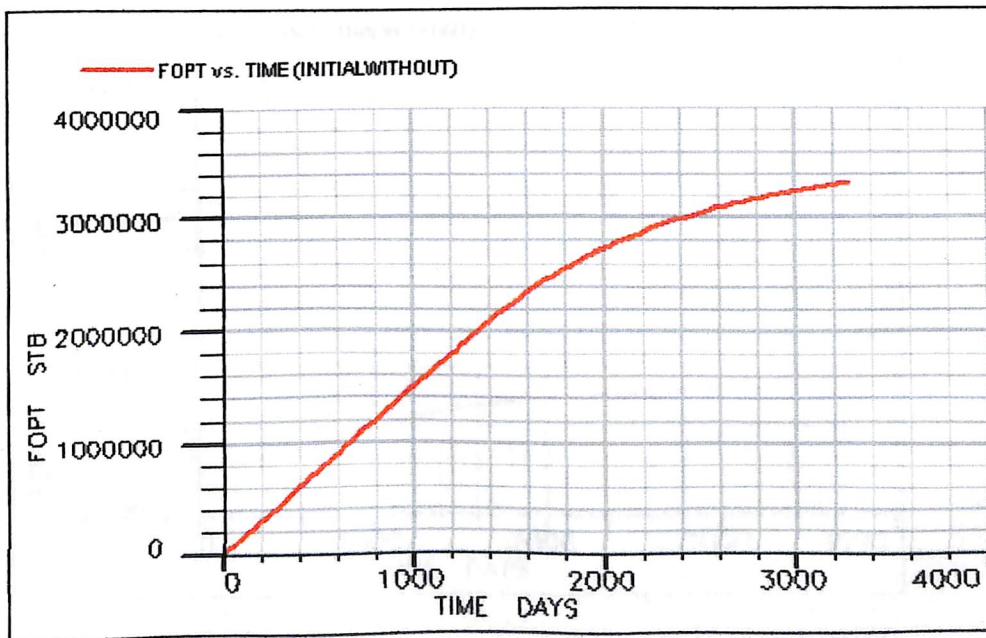
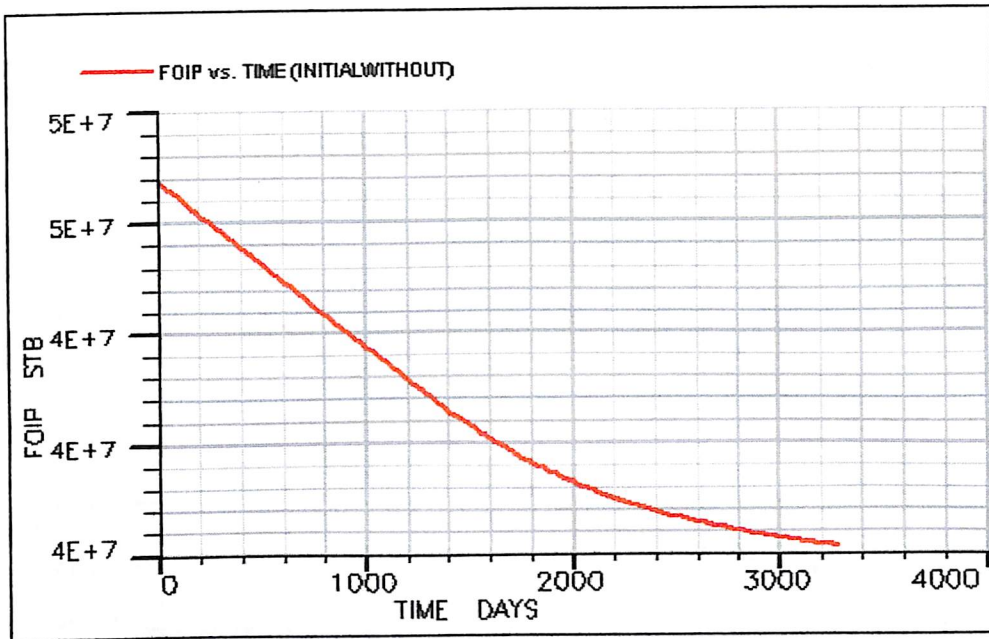
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5. RESULTS

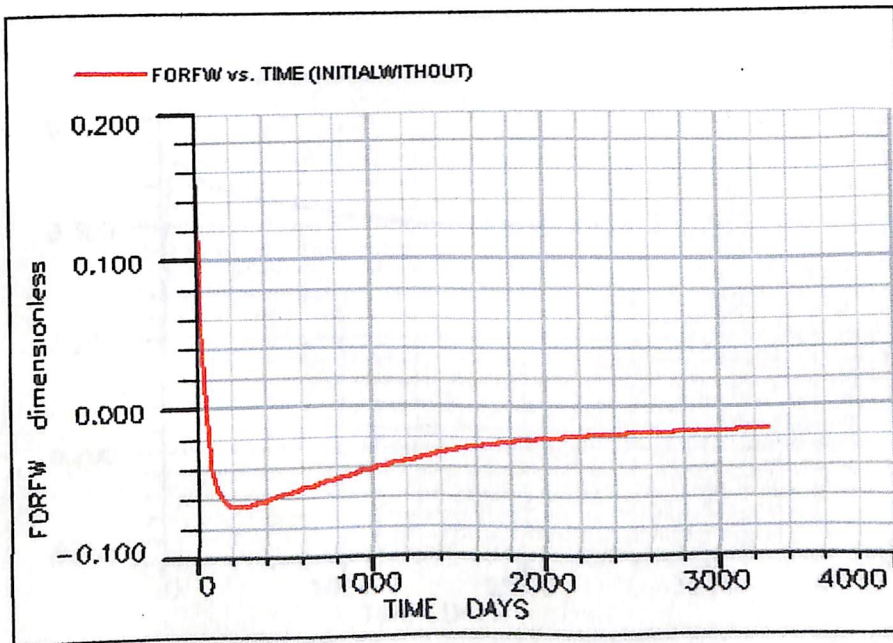
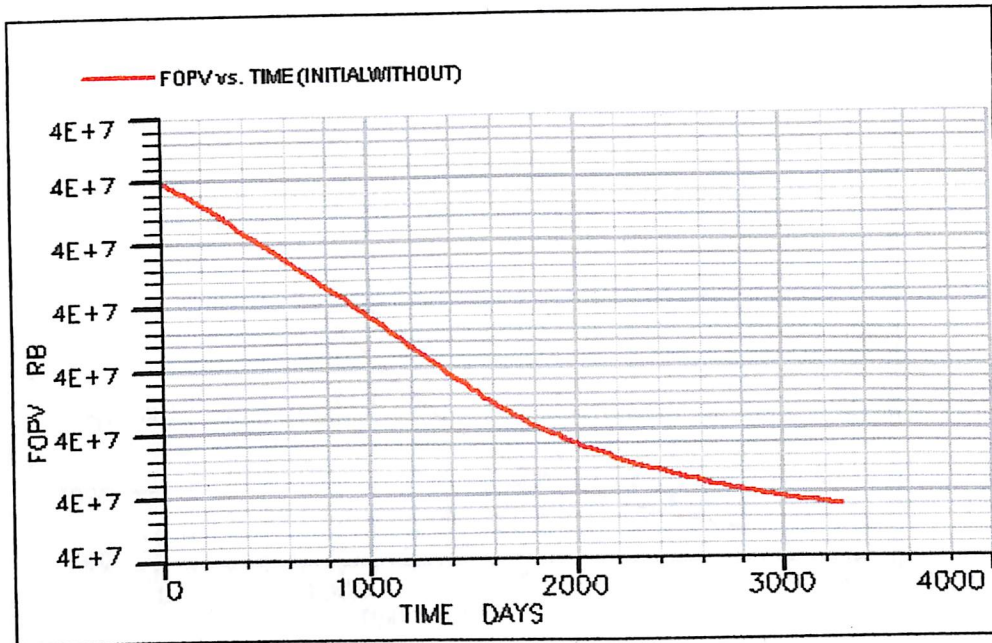
BEFORE WATER INJECTION

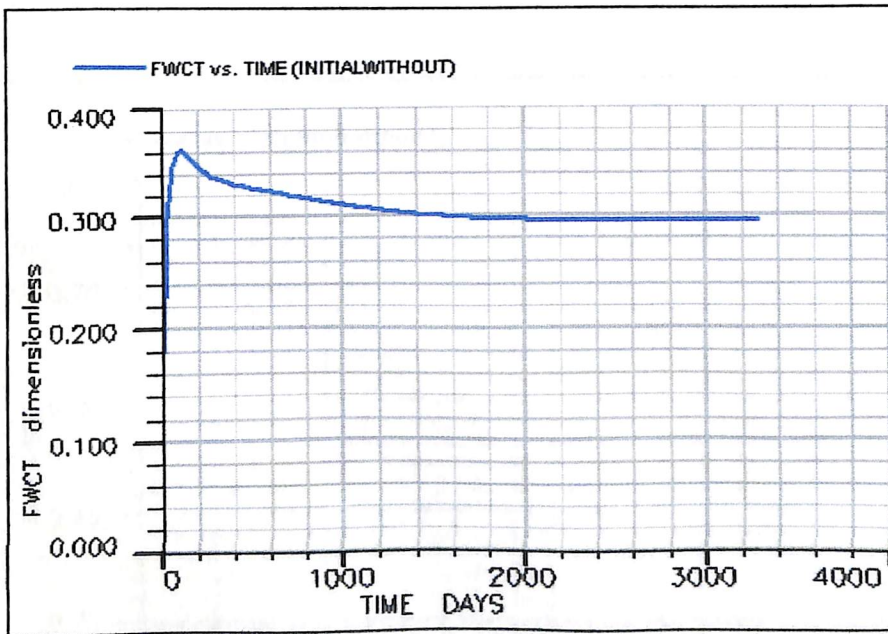
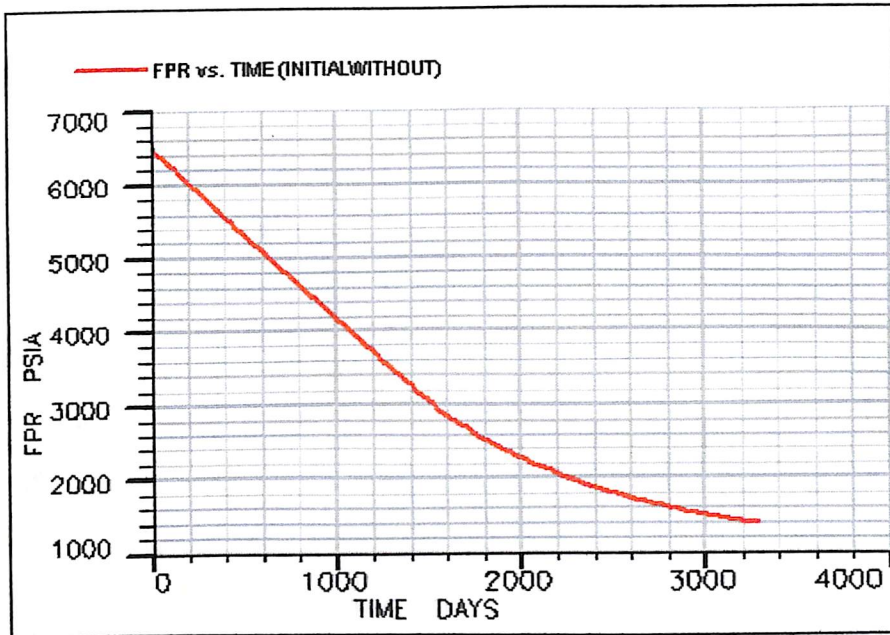


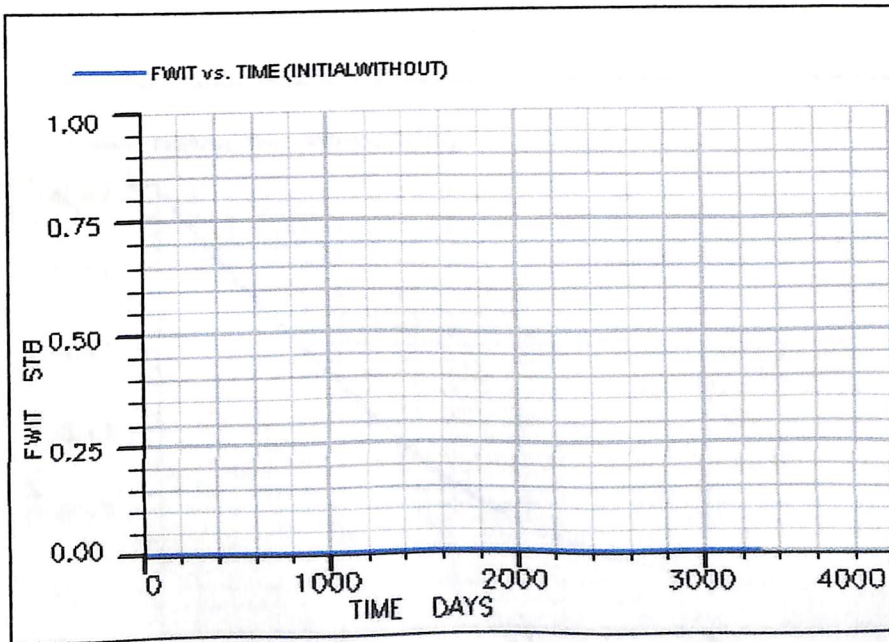
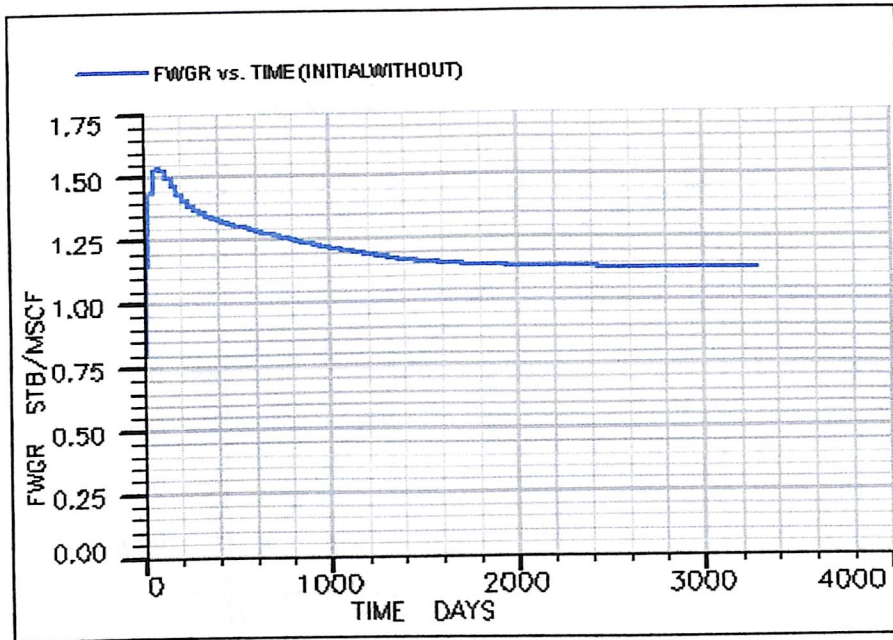
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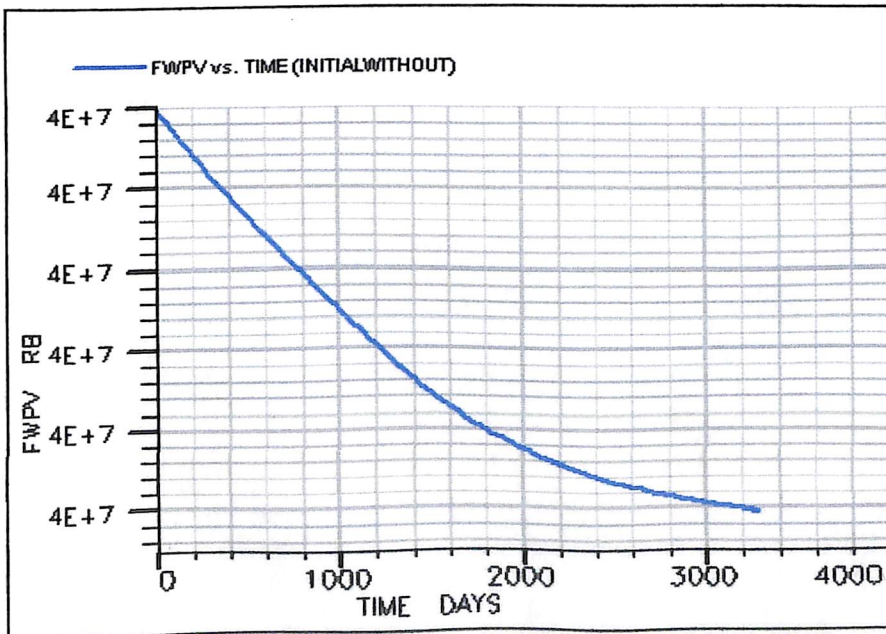
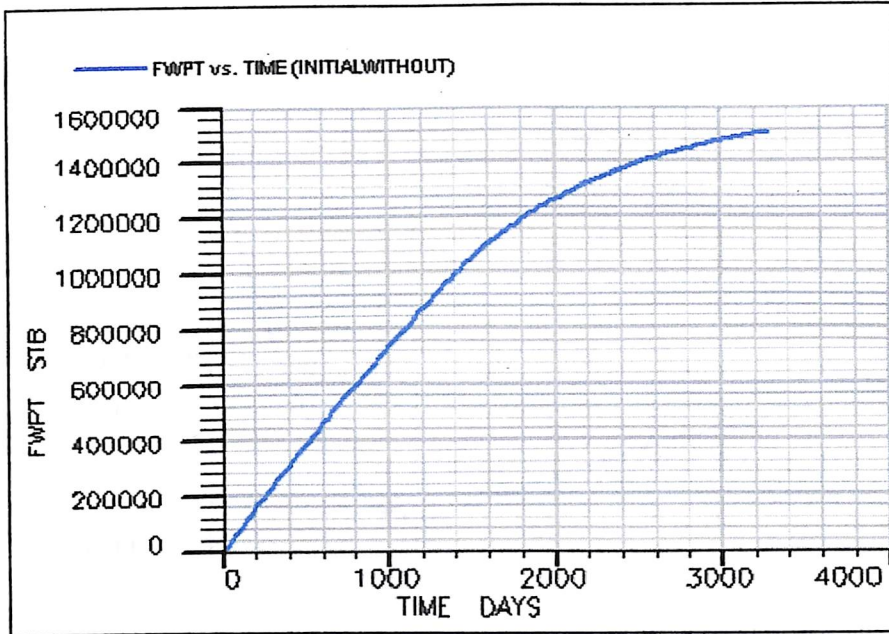


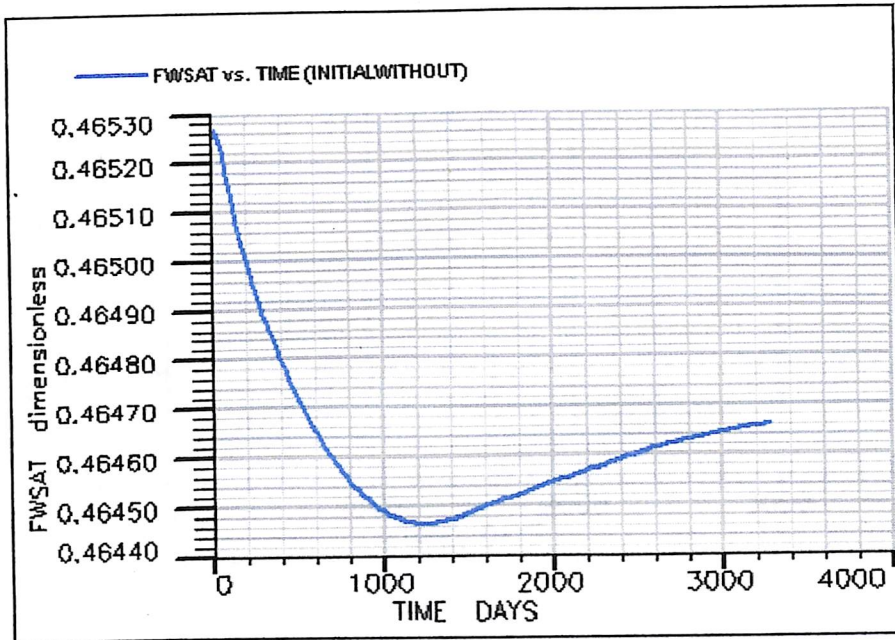
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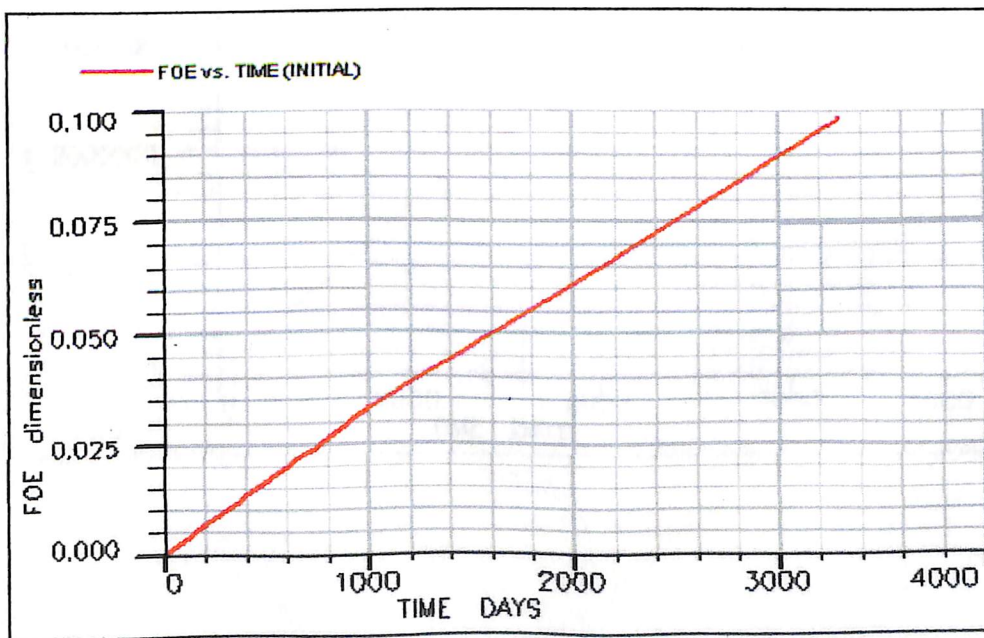
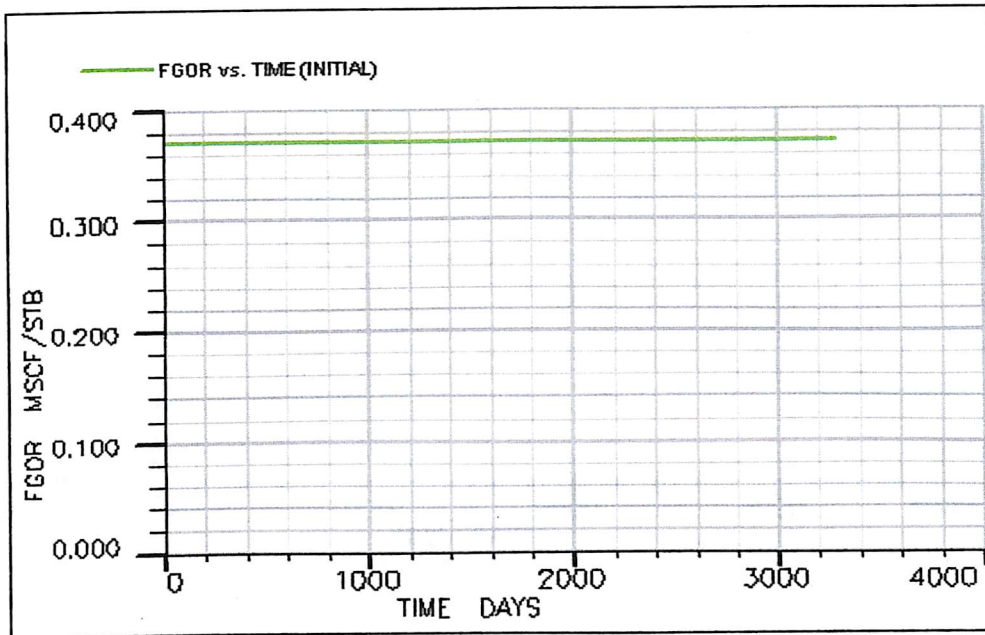




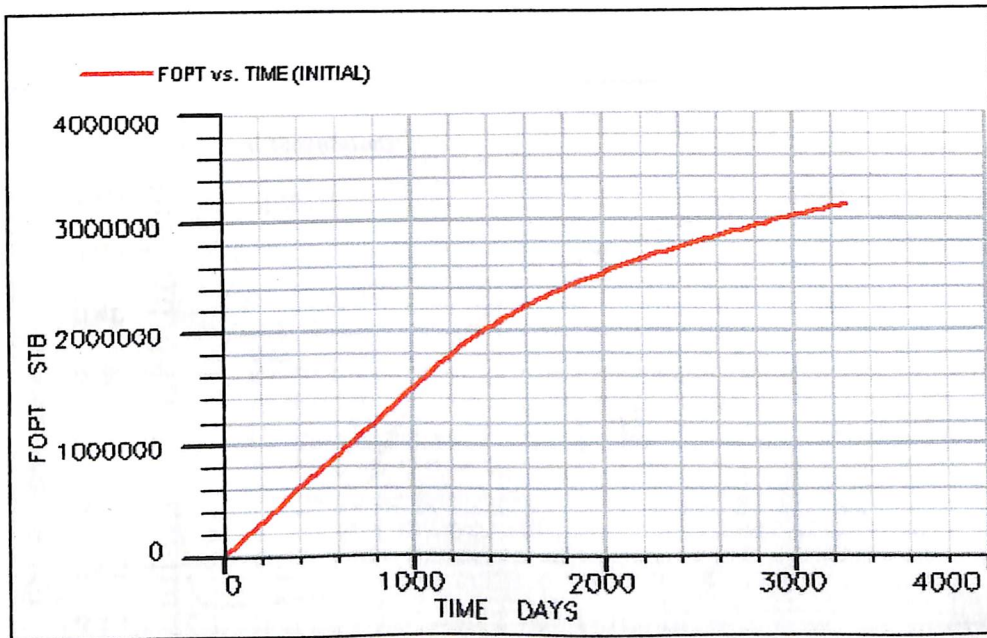
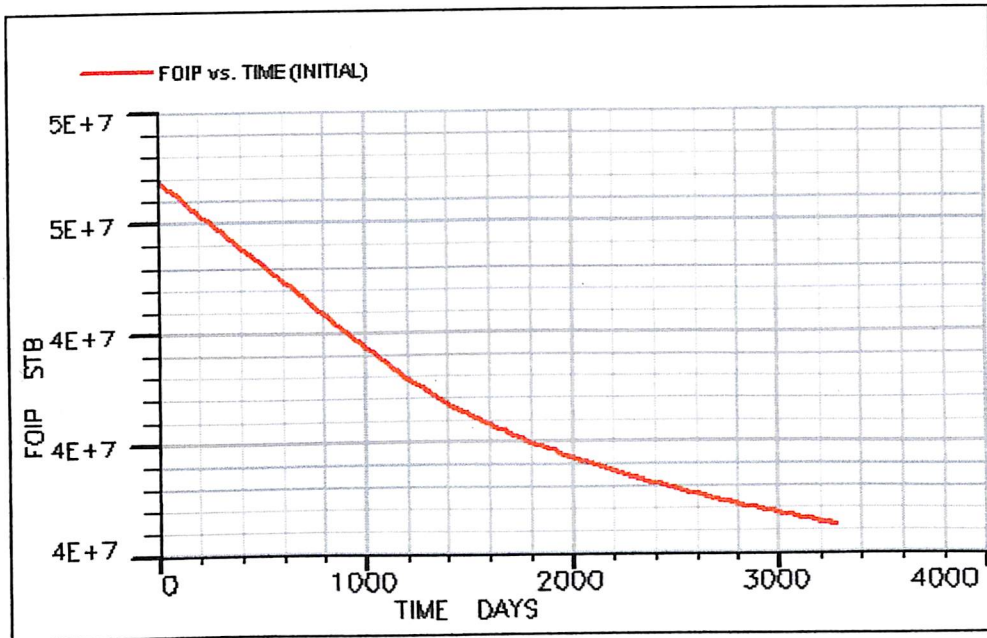




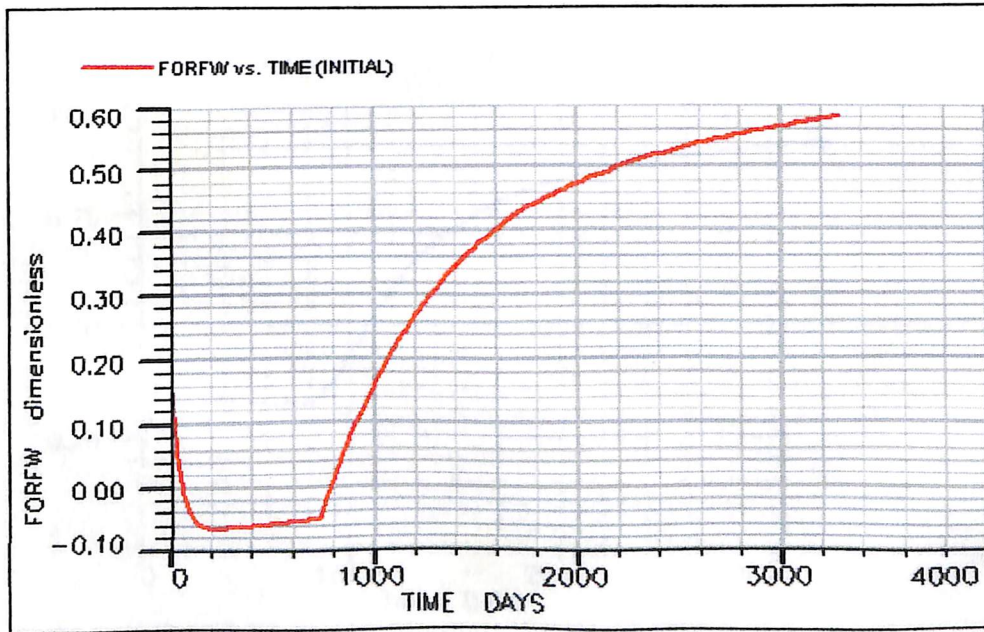
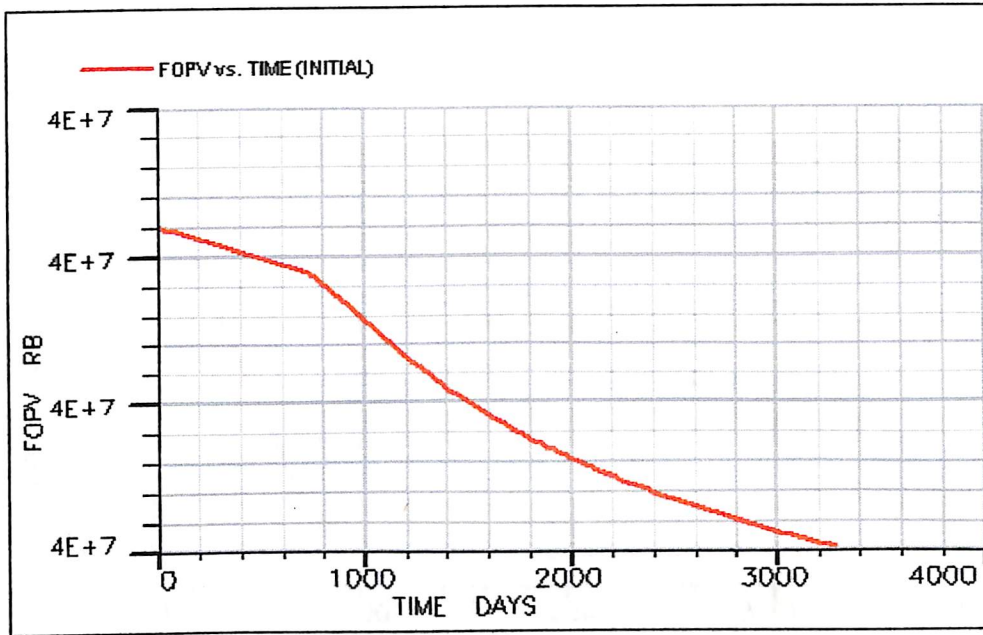
AFTER WATERFLOODING



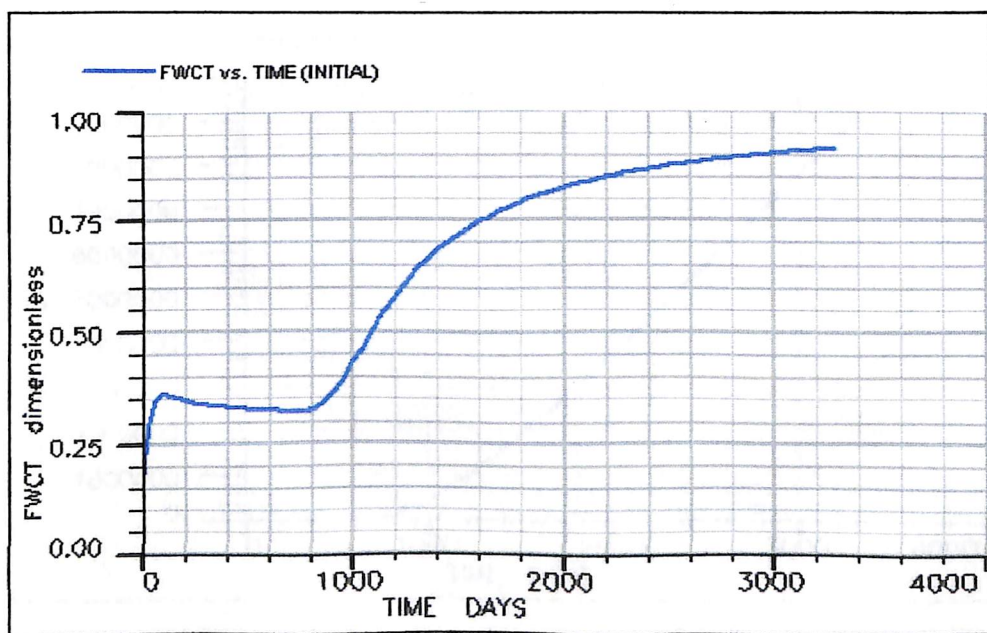
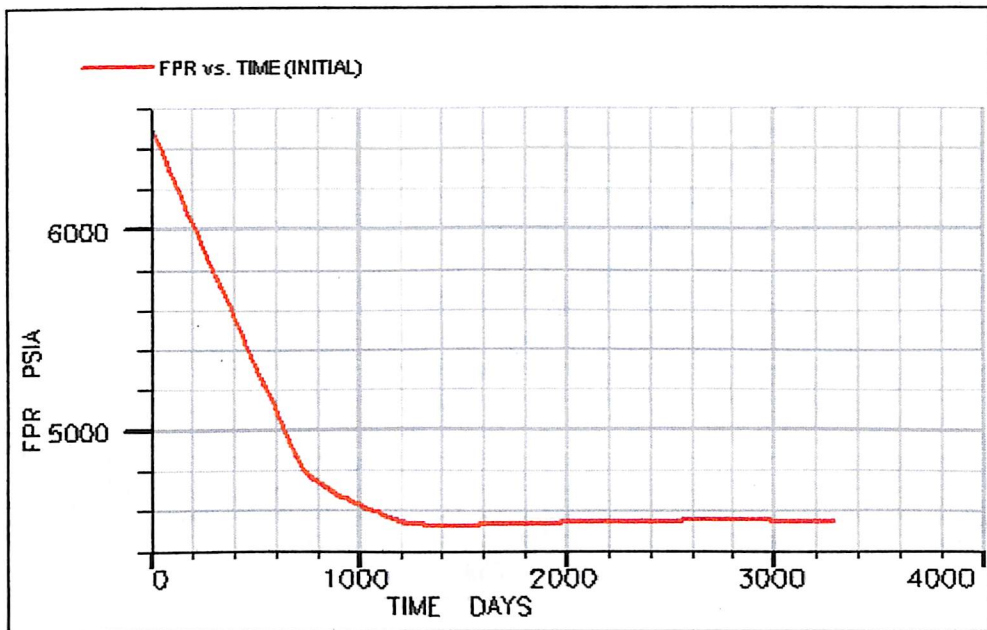
University of Petroleum & Energy Studies



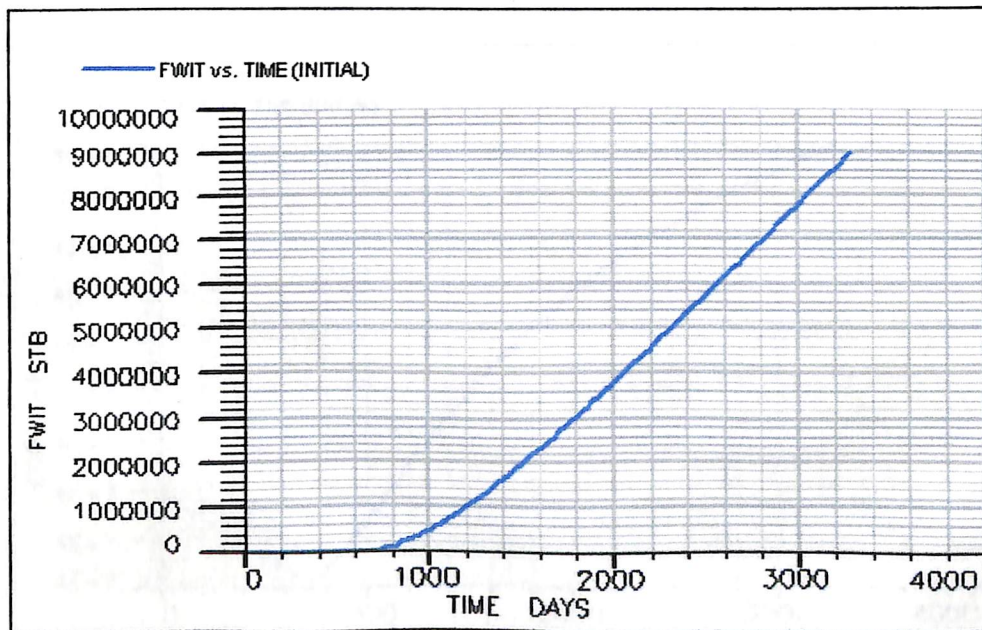
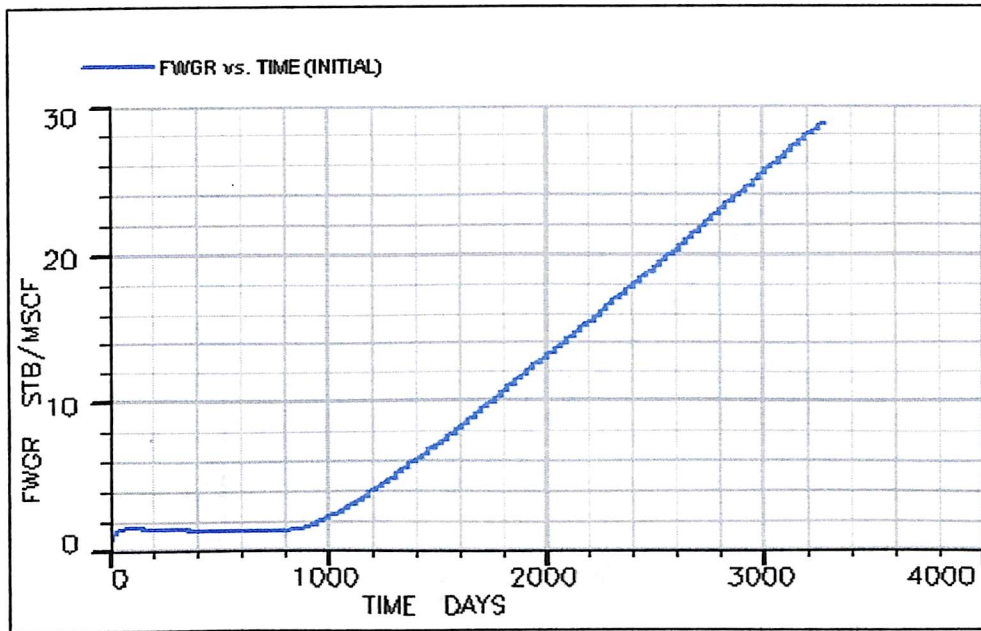
University of Petroleum & Energy Studies



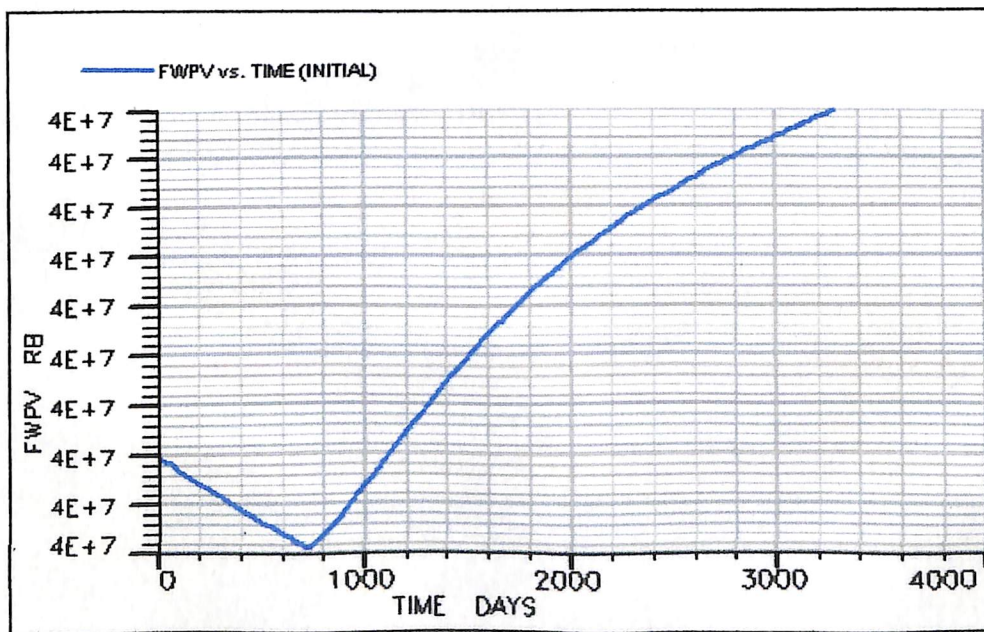
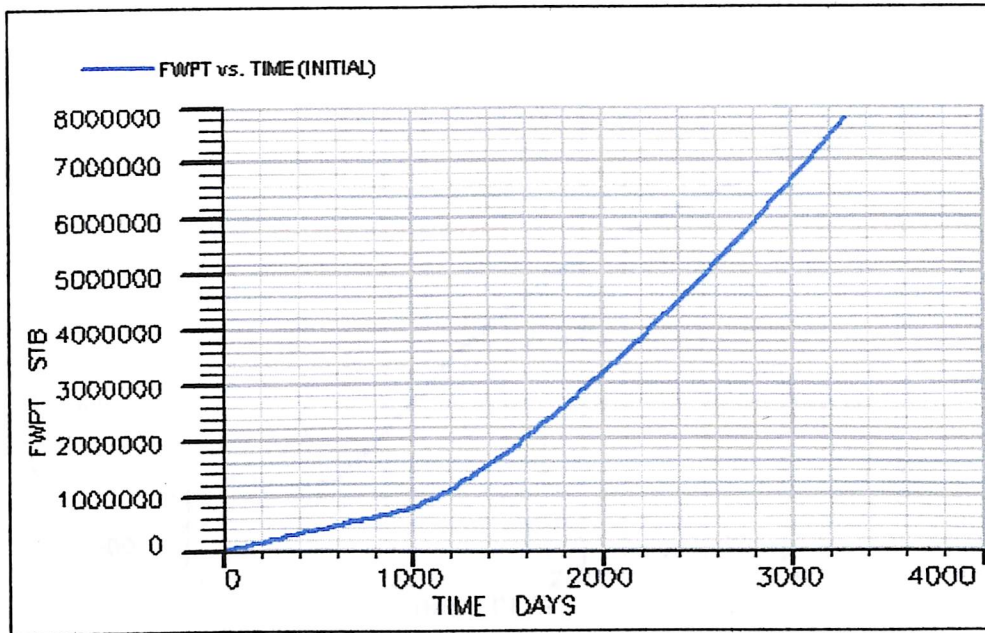
University of Petroleum & Energy Studies



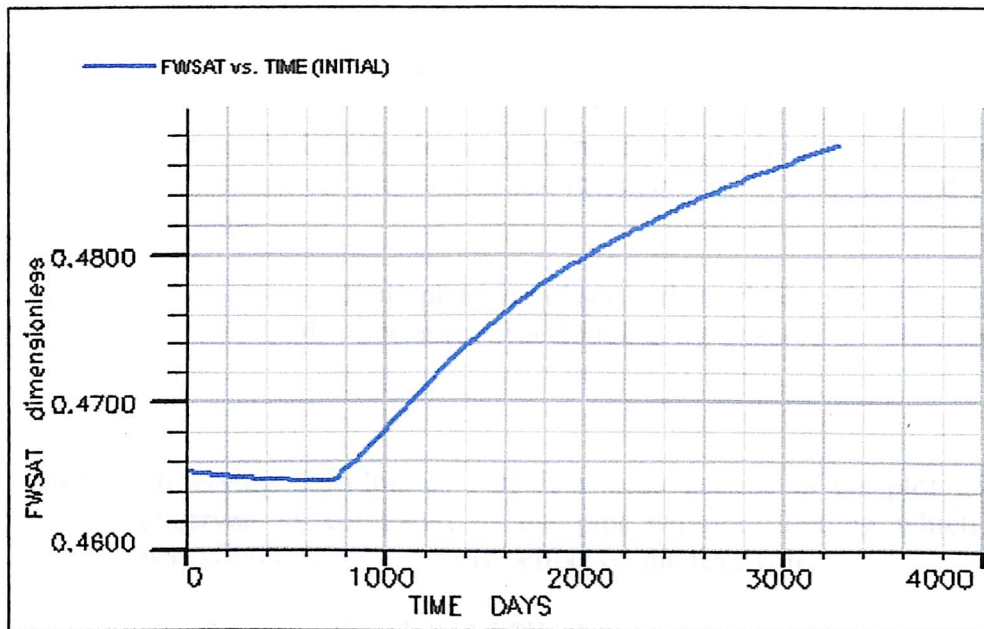
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It is observed that water retention in the reservoir is 0.485 as compared to the initial value of 0.465.

A comparative result from graphs are made and it clearly shows that the waterflooding project will increase the recovery with given flow rates and injection rates. So the project is economically evaluation for its feasibility in field operations.

6. COMPARATIVE STUDY AND CONCLUSION

It must be noted that that in the 9 year prediction run the reservoir pressure did not fall below bubble point pressure. The production rate of the formation doesn't change before and after the implementation of waterflooding program.

- i.) Comparing FOGR plot we observe that in both scenarios it remains constant, since reservoir pressure is above bubble point pressure and production rate constant.
- ii.) If we observe FOE plots we observe that without flooding the recovery³ is 7.3% of OOIP. Scenario with flooding we observe an additional recovery of 2.6%.
- iii.) Observing the plots of FOPV, a steep decline in the plot with flooding is observed as compared to the plot without flooding which explains that waterflooding has a positive effect on the reservoir.
- iv.) On observing the plot of FPR after waterflooding we see that, the reservoir pressure has been stabilized after a certain period of time which is not the same in the case of without waterflooding.
- v.) Post waterflooding it is observed that water saturation in the reservoir has increased to 0.4875 as compared to the initial value of 0.4655.

A comparative result from graphs are made and it clearly shows that the waterflooding project will enhance the recovery with given flow rates and injection rates. So the project needs an economic evaluation for its feasibility in field operation.

REFERENCES

- i.) S. E. Buckley and M. C. Leverett "Mechanism of fluid displacements in sands", Trans. AIME, (1942), p.iv.
- ii.) H. Dykstra and R. L. Parsons, "The prediction of oil recovery by water flood", secondary recovery of oil in united states, Second edition, (New York: American Petroleum Institute, 1950), p.3.
- iii.) C. E. Johnson, Jr., "Prediction of oil recovery by water flood- A simplified graphical treatment", Trans. AIME, (1956), p.39.
- iv.) F. E. Suder and J. C. Calhoun, Jr., "Water-flood Calculations", Drilling and Production practice, API, (1949), p.2.
- v.) P. S. Ache, "Inclusion of radial flow in Use of permeability distributions in water flood calculations", paper presented before 32nd Annual meeting of SPE of AIME, Oct. 6-9, 1957, Dallas, Texas, p.6.
- vi.) Dimensionless Equations for Water flood history matching (SPE 25521), 1992 Stein, M. H. Carlson, p.10.
- vii.) Simulation studies of Water flooding practice – Ferreira .H, Mamora .D. D and startzman .R .A, p.9

APPENDIX A – OUTPUT DATA FILE FOR WATER FLOODING

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Annex | Modification date | Update date | baseline
=====|=====|=====|=====
ECLIPSE | 29-SEP-2005 19:01:55 | 06-OCT-2005 09:22:21 | S:\2005a_1_w39i
system | 14-SEP-2005 12:31:07 | 24-SEP-2005 04:17:36 | S:\2005a_1_w39
utility | 27-JAN-2005 12:36:55 | 24-SEP-2005 04:17:40 | S:\2005a_1_w39
```

1

***** ECHO OF INPUT DATA FOR RUN initial

```
0: RUNSPEC
0:
0: TITLE
0: INITIAL
0:
0: DIMENS
0: 20 20 1 /
0:
0: OIL
0:
0: WATER
0:
0: FIELD
0:
0: WELLDIMS
0: 5 1 2 4/
0:
0: START
0: 1 'JAN' 2007 /
0:
0: UNIFOUT
0:
0: --
0:
0: GRID
0:
0: BOX
0: 1 20 1 20 1 1 /
0:
0: DXV
0: 20*500 /
0:
0: DYV
0: 20*500 /
0:
0: DZ
0: 38.2 37.4 36.6 36.0 35.8 36.0 36.6 37.3 38.0 38.5 38.7 38.7 38.6 38.6
37.6 36.7 36.2 36.3 37.0 37.9
0: 39.1 40.1 41.0 41.2 41.1 40.8 38.5 37.5 36.5 35.8 36.4 37.5 38.9 40.4
41.9 43.2 43.4 43.1 42.6 38.1
0: 37.3 36.4 35.8 36.6 38.0 39.5 41.1 42.8 44.3 44.6 44.3 44.0 37.3 37.0
36.6 36.6 37.3 38.4 39.7 41.1
0: 42.5 43.8 44.5 44.8 45.0 36.2 36.6 37.0 37.4 38.1 38.8 39.7 40.6 41.7
42.8 43.8 44.8 45.6 34.8 36.0
0: 37.1 38.0 38.6 39.0 39.3 39.7 40.4 41.4 42.8 44.4 46.0 32.9 35.1 37.1
38.5 39.1 39.0 38.7 38.6 38.8
0: 39.7 41.4 43.7 46.2 30.6 33.8 36.7 38.7 39.1 38.5 37.8 37.3 37.1 37.7
39.8 42.9 46.0 28.7 32.1 35.3
0: 37.7 38.0 37.3 36.6 36.0 35.7 36.2 38.6 42.0 45.3 27.3 30.1 32.7 34.7
35.4 35.2 34.9 34.8 35.0 36.0
0: 38.2 41.1 44.2 25.8 27.8 29.8 31.3 32.3 32.8 33.1 33.6 34.4 35.7 37.8
40.2 42.7 24.0 25.5 27.0 28.2
0: 38.2 37.4 36.6 36.3 37.0 35.8 36.0 36.6 37.3 38.0 38.5 38.7 38.7 38.6 38.6
37.6 36.7 36.2 36.3 37.0 37.9
0: 39.1 40.1 41.0 41.2 41.1 40.8 38.5 37.5 36.5 35.8 36.4 37.5 38.9 40.4
41.9 43.2 43.4 43.1 42.6 38.1
```


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0: 37.3 36.4 35.8 36.6 38.0 39.5 41.1 42.8 44.3 44.6 44.3 44.0 37.3 37.0
36.6 36.6 37.3 38.4 39.7 41.1
0: 42.5 43.8 44.5 44.8 45.0 36.2 36.6 37.0 37.4 38.1 38.8 39.7 40.6 41.7
42.8 43.8 44.8 45.6 34.8 36.0
0: 37.1 38.0 38.6 39.0 39.3 39.7 40.4 41.4 42.8 44.4 46.0 32.9 35.1 37.1
38.5 39.1 39.0 38.7 38.6 38.8
0: 39.7 41.4 43.7 46.2 30.6 33.8 36.7 38.7 39.1 38.5 37.8 37.3 37.1 37.7
39.8 42.9 46.0 28.7 32.1 35.3
0: 37.7 38.0 37.3 36.6 36.0 35.7 36.2 38.6 42.0 45.3 27.3 30.1 32.7 34.7
35.4 35.2 34.9 34.8 35.0 36.0
0: 38.2 41.1 44.2 25.8 27.8 29.8 31.3 32.3 32.8 33.1 33.6 34.4 35.7 37.8
40.2 42.7 24.0 25.5 27.0 28.2
0: 38.2 37.4 36.6 36.0 35.8 36.0 36.6 37.3 38.0 38.5 38.7 38.7 38.6 38.6
37.6 36.7 36.2 36.3 37.0 37.9
0: 39.1 40.1 41.0 41.2 41.1 40.8 38.5 37.5 36.5 35.8 36.4 37.5 38.9 40.4
41.9 43.2 43.4 43.1 42.6 38.1
0: 37.3 36.4 35.8 36.6 38.0 39.5 41.1 42.8 44.3 44.6 44.3 44.0 37.3 37.0
36.6 36.6 37.3 38.4 39.7 41.1
0: 42.5 43.8 44.5 44.8 45.0 36.2 36.6 37.0 37.4 38.1 38.8 39.7 40.6 41.7
42.8 43.8 44.8 45.6 34.8 36.0
0:
0: /
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0: PORO
0:
0: 0.16 0.14 0.12 0.1 0.08 0.09 0.1 0.11 0.12 0.13 0.16 0.14 0.12 0.1 0.08 0.09 0.1 0.11
0.12 0.13
0: 0.16 0.14 0.12 0.1 0.09 0.09 0.1 0.11 0.12 0.13 0.16 0.14 0.12 0.1 0.09 0.09 0.1 0.11
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0: 0.15 0.14 0.12 0.1 0.10 0.09 0.1 0.11 0.12 0.13 0.15 0.14 0.12 0.1 0.10 0.09 0.1 0.11
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0: 0.15 0.14 0.12 0.1 0.10 0.09 0.1 0.11 0.12 0.13 0.15 0.14 0.12 0.1 0.10 0.09 0.1 0.11
0.12 0.13
0: /
0:
0: PERMX
0:
0: 150 150 8*160 3*40 4*160 2*80 146
0: 140 150 8*160 3*50 4*134 2*68 147

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0: 130 150 8*165 3*40 4*142 2*75 149
0: 120 150 8*170 3*55 4*160 2*77 157
0: 110 150 8*175 3*40 4*132 2*64 152
0: 100 150 8*175 3*34 4*135 2*58 156
0: 90 150 8*160 3*47 4*144 2*74 133
0: 80 150 8*160 3*54 4*154 2*86 133
0: 60 150 8*175 3*70 4*160 2*69 162
0: 50 150 8*175 3*30 4*150 2*80 146
0: 150 150 8*160 3*40 4*160 2*80 146
0: 140 150 8*160 3*50 4*134 2*68 147
0: 130 150 8*165 3*40 4*142 2*75 149
0: 120 150 8*170 3*55 4*160 2*77 157
0: 110 150 8*175 3*40 4*132 2*64 152
0: 100 150 8*175 3*34 4*135 2*58 156
0: 90 150 8*160 3*47 4*144 2*74 133
0: 80 150 8*160 3*54 4*154 2*86 133
0: 60 150 8*175 3*70 4*160 2*69 162
0: 50 150 8*175 3*30 4*150 2*80 146

0: /

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0: PERMY

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0: 150 150 8*160 3*140 4*160 2*80 146
0: 140 150 8*160 3*150 4*134 2*68 147
0: 130 150 8*165 3*140 4*142 2*75 149
0: 120 150 8*170 3*155 4*160 2*77 157
0: 110 150 8*175 3*140 4*132 2*64 152
0: 100 150 8*175 3*134 4*135 2*58 156
0: 90 150 8*160 3*147 4*144 2*74 133
0: 80 150 8*160 3*154 4*154 2*86 133
0: 60 150 8*175 3*170 4*160 2*69 162
0: 50 150 8*175 3*130 4*150 2*80 146
0: 150 150 8*160 3*140 4*160 2*80 146
0: 140 150 8*160 3*150 4*134 2*68 147
0: 130 150 8*165 3*140 4*142 2*75 149
0: 120 150 8*170 3*155 4*160 2*77 157
0: 110 150 8*175 3*140 4*132 2*64 152
0: 100 150 8*175 3*134 4*135 2*58 156
0: 90 150 8*160 3*147 4*144 2*74 133
0: 80 150 8*160 3*154 4*154 2*86 133
0: 60 150 8*175 3*170 4*160 2*69 162
0: 50 150 8*175 3*130 4*150 2*80 146

0: /

0: PERMZ

0:

0: 400*150 /

0:

0: ENDBOX

0: /

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0: TOPS

0:

0: 7000 7000 7000 7000 7000 7000 7000 7000 7000 7000 7000 7000 7000 7000 7000 7000
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7000 7000 7000
0:
0: /
0:
0: INIT
0:
0: --*****
0: EDIT
0:
0: --*****
0: PROPS
0:
0: SWOF
0: -- Sw          krw          kro          Pcwo
0: 0.20          0.000000        0.900000        0
0: 0.25          0.000364        0.709187        0
0: 0.30          0.002536        0.544963        0
0: 0.35          0.007892        0.405962        0
0: 0.40          0.017660        0.290741        0
0: 0.45          0.032987        0.197760        0
0: 0.50          0.054960        0.125368        0
0: 0.55          0.084625        0.071765        0
0: 0.60          0.122991        0.034959        0
0: 0.65          0.171041        0.012686        0
0: 0.70          0.229732        0.002243        0
0: 0.75          0.300000        0.000000        0
0: /
0:
0:
0: -- Specifies PVT properties of OIL
0: PVDO
0: 400 1.012 1.16
0: 1200 1.0040 1.164
0: 2000 0.9960 1.167
0: 2800 0.9880 1.172
0: 3600 0.9802 1.177
0: 4400 0.9724 1.181
0: 5200 0.9646 1.185
0: 5600 0.9607 1.19
0: /
0:
0: PVTW
0: 1050          1          2.67E-06        0.56341        1.20E-07 /
0:
0:
0: RSCONST
0: 0.37 1050 /
0:
0: DENSITY
0: 47 63.0200 /

```

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```
0:
0: ROCK
0: 1050.0      5.0E-06 /
0:
0: -----
0: REGIONS
0:
0: -----
0: SOLUTION
0:
0: EQUIL
0: 7020      6500      7020      0      0 /
0:
0:
0: -----
0: SUMMARY
0:
0: -- Average pressure for field.
0: FPR
0:
0: -- Oil production total
0: FOPT
0:
0: -- Water injection total of field
0: FWIT
0:
0: --Water cut
0: FWCT
0:
0: --OIL IN PLACE
0: FOIP
0:
0: -- FORMATION WATER SATURATION
0: FWSAT
0:
0: --Water Reservoir Volume in Place
0: FWIPR
0:
0: --Fraction of total oil produced by water influx
0: FORFW
0:
0: --FORM OIL PORE VOL
0: FOPV
0:
0: --FORM WATER PORE VOL
0: FWPV
0:
0: --OIL RECOVERY
0: FOE
0:
0: --GOR
0: FGOR
0:
0: --Water production
0: FWPT
0:
0: -- Average pressure for field.
0: FPR
0:
0: -- Oil production total
0: FOPT
0:
0: -- Water injection total of field
0: FWIT
0:
0: --Water production
0: FWPT
0:
0: -- WATER GAS RATIO
0: FWGR
0:
```

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```

0: EXCEL
0:
0: -----
0: SCHEDULE
0:
0: WELSPECS
0: P G1 10 10 7015 'OIL' /
0: /
0:
0:
0: COMPDAT
0: P 10 10 1 1 'OPEN' 2* 0.2 /
0: /
0:
0: WCONPROD
0: P 'OPEN' ORATE 1500      4*      1000/
0: /
0:
0: TSTEP
0:
0: 31 28      31      30      31      30      31      31      30      31      30      31
0: 31 28      31      30      31      30      31      31      30      31      30      31
0: /
0:
0: WELSPECS
0: I1 G2 7 10 7015 'WAT' /
0: I2 G2 13 10 7015 'WAT' /
0: I3 G2 10 7 7015 'WAT' /
0: I4 G2 10 13 7015 'WAT' /
0: /
0:
0: COMPDAT
0: I1 7 10 1 1 'OPEN' 2* 0.2 /
0: I2 13 10 1 1 'OPEN' 2* 0.2 /
0: I3 10 7 1 1 'OPEN' 2* 0.2 /
0: I4 10 13 1 1 'OPEN' 2* 0.2 /
0: /
0:
0: WCONPROD
0: P 'OPEN' ORATE 1500      4*      1000/
0: /
0:
0: WCONINJE
0: I1 WATER OPEN RATE 4000 1*      5000/
0: I2 WATER OPEN RATE 4000 1*      5000/
0: I3 WATER OPEN RATE 4000 1*      5000/
0: I4 WATER OPEN RATE 4000 1*      5000/
0: /
0:
0: TSTEP
0:
0: 31 28      31      30      31      30      31      31      30      31      30      31
0: 31 28      31      30      31      30      31      31      30      31      30      31
0: 31 28      31      30      31      30      31      31      30      31      30      31
0: 31 28      31      30      31      30      31      31      30      31      30      31
0: 31 28      31      30      31      30      31      31      30      31      30      31
0: 31 28      31      30      31      30      31      31      30      31      30      31
0: /
0:
0: END
0:
0:
0:
0:

```

```

***** END OF INPUT DATA FOR RUN initial
1 READING RUNSPEC

```

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- 2 READING TITLE
- 3 READING DIMENS
- 4 READING OIL
- 5 READING WATER
- 6 READING FIELD
- 7 READING WELLDIMS
- 8 READING START
- 9 READING UNIFOUT
- 10 READING GRID

1

LIST OF ECLIPSE 100 SPECIAL OPTIONS

=====

POLYMER FLOOD	-	-	-	-	-	-	-	-	-	NOT AVAILABLE
NETWORKS	-	-	-	-	-	-	-	-	-	NOT AVAILABLE
LOCAL GRID REFINEMENT/COARSENING	-	-	-	-	-	-	-	-	-	AVAILABLE
FLUX BOUNDARY OPTION	-	-	-	-	-	-	-	-	-	NOT AVAILABLE
SOLVENT FLOOD MODEL	-	-	-	-	-	-	-	-	-	NOT AVAILABLE
GAS FIELD OPERATIONS MODEL	-	-	-	-	-	-	-	-	-	AVAILABLE
WELLBORE FRICTION OPTION	-	-	-	-	-	-	-	-	-	NOT AVAILABLE
GI-MODEL	-	-	-	-	-	-	-	-	-	NOT AVAILABLE
SURFACTANT FLOOD	-	-	-	-	-	-	-	-	-	NOT AVAILABLE
GAS LIFT OPTIMISATION	-	-	-	-	-	-	-	-	-	AVAILABLE
PARALLEL OPTIONS	-	-	-	-	-	-	-	-	-	NOT AVAILABLE
ENVIRONMENTAL TRACERS	-	-	-	-	-	-	-	-	-	NOT AVAILABLE
COAL BED METHANE OPTION	-	-	-	-	-	-	-	-	-	AVAILABLE
MULTI-SEGMENT WELL OPTION	-	-	-	-	-	-	-	-	-	NOT AVAILABLE
RESERVOIR COUPLING	-	-	-	-	-	-	-	-	-	AVAILABLE
FOAM MODEL	-	-	-	-	-	-	-	-	-	NOT AVAILABLE
GAS QUALITY CONTROL OPTION	-	-	-	-	-	-	-	-	-	AVAILABLE
UNCODED GRADIENTS	-	-	-	-	-	-	-	-	-	NOT AVAILABLE

THE PRESENT PROGRAM/PASSWORD COMBINATION EXPIRES ON 4/DEC/2008

1

- 12 READING BOX
- 13 READING DXV
- 14 READING DYV
- 15 READING DZ
- 16 READING PORO
- 17 READING PERMX
- 18 READING PERMY
- 19 READING PERMZ
- 20 READING ENDBOX

```
@--WARNING AT TIME 0.0 DAYS ( 1-JAN-2007):
@          SPURIOUS DATA BEFORE TOPS      KEYWORD
@          /
```

- 21 READING TOPS
- 22 READING INIT
- 23 READING EDIT

```
@--MESSAGE AT TIME 0.0 DAYS ( 1-JAN-2007):
@          NEITHER OLDTRAN,OLDTRANR NOR NEWTRAN SPECIFIED
@          BLOCK CENTRE TRANSMISSIBILITIES TO BE CALCULATED
@          USING OLDTRAN
```

- 24 READING PROPS

```
@--COMMENT AT TIME 0.0 DAYS ( 1-JAN-2007):
@          NO NON-NEIGHBOUR CONNECTIONS FOUND
```

```
@--MESSAGE AT TIME 0.0 DAYS ( 1-JAN-2007):
@          NUMBER OF ACTIVE CELLS IS      400
```

```
@--MESSAGE AT TIME 0.0 DAYS ( 1-JAN-2007):
@          PROBLEM REQUIRES      0.571 MEGABYTES
@          1497 ( BYTES PER ACTIVE CELL )
```

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@--MESSAGE AT TIME 0.0 DAYS (1-JAN-2007):
@ 48522 CHARACTER VARIABLES USED
25 READING SWOF
26 READING PVDO
27 READING PVTW

@--WARNING AT TIME 0.0 DAYS (1-JAN-2007):
@ SPURIOUS DATA BEFORE RSCONST KEYWORD
@
28 READING RSCONST
29 READING DENSITY
30 READING ROCK
31 READING REGIONS
32 READING SOLUTION
33 READING EQUIL
34 READING SUMMARY
35 READING FPR
36 READING FOPT
37 READING FWIT
38 READING FWCT
39 READING FOIP
40 READING FWSAT
41 READING FWIPR

@--WARNING AT TIME 0.0 DAYS (1-JAN-2007):
@ UNRECOGNISED KEYWORD FWIPR IN SUMMARY FILE SPECIFICATION
42 READING FORFW
43 READING FOPV
44 READING FWPV
45 READING FOE
46 READING FGOR
47 READING FWPT
48 READING FPR
49 READING FOPT
50 READING FWIT
51 READING FWPT
52 READING FWGR
53 READING EXCEL
54 READING SCHEDULE
55 READING WELSPECS
56 READING COMPDAT
57 READING WCONPROD
58 READING TSTEP

1
***** 1
SIMULATE AT 0.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 0 1 JAN 2007 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 1 TIME= 1.00 DAYS (+1.0 DAYS INIT 1 ITS) (2-JAN-2007)
PAV= 6497.9 PSIA WCT=0.163 GOR= 0.37 MSCF/STB WGR= 0.5263 STB/MSCF
STEP 2 TIME= 4.00 DAYS (+3.0 DAYS MAXF 1 ITS) (5-JAN-2007)
PAV= 6492.3 PSIA WCT=0.180 GOR= 0.37 MSCF/STB WGR= 0.5926 STB/MSCF
STEP 3 TIME= 13.00 DAYS (+9.0 DAYS MAXF 2 ITS) (14-JAN-2007)
PAV= 6474.5 PSIA WCT=0.228 GOR= 0.37 MSCF/STB WGR= 0.7961 STB/MSCF
STEP 4 TIME= 31.00 DAYS (+18.0 DAYS REPT 2 ITS) (1-FEB-2007)
PAV= 6435.0 PSIA WCT=0.299 GOR= 0.37 MSCF/STB WGR= 1.1547 STB/MSCF

1
***** 2
SIMULATE AT 31.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 1 1 FEB 2007 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

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```
*****
STEP 5 TIME= 59.00 DAYS ( +28.0 DAYS REPT 2 ITS) (1-MAR-2007)
PAV= 6368.7 PSIA WCT=0.349 GOR= 0.37 MSCF/STB WGR= 1.4470 STB/MSCF
1
***** 3
SIMULATE AT 59.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 2 1 MAR 2007 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 6 TIME= 90.00 DAYS ( +31.0 DAYS REPT 2 ITS) (1-APR-2007)
PAV= 6293.5 PSIA WCT=0.363 GOR= 0.37 MSCF/STB WGR= 1.5386 STB/MSCF
1
***** 4
SIMULATE AT 90.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 3 1 APR 2007 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 7 TIME= 120.00 DAYS ( +30.0 DAYS REPT 1 ITS) (1-MAY-2007)
PAV= 6220.9 PSIA WCT=0.362 GOR= 0.37 MSCF/STB WGR= 1.5334 STB/MSCF
1
***** 5
SIMULATE AT 120.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 4 1 MAY 2007 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 8 TIME= 151.00 DAYS ( +31.0 DAYS REPT 2 ITS) (1-JUN-2007)
PAV= 6146.4 PSIA WCT=0.357 GOR= 0.37 MSCF/STB WGR= 1.5000 STB/MSCF
1
***** 6
SIMULATE AT 151.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 5 1 JUN 2007 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 9 TIME= 181.00 DAYS ( +30.0 DAYS REPT 1 ITS) (1-JULY-2007)
PAV= 6074.8 PSIA WCT=0.352 GOR= 0.37 MSCF/STB WGR= 1.4656 STB/MSCF
1
***** 7
SIMULATE AT 181.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 6 1 JULY 2007 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 10 TIME= 212.00 DAYS ( +31.0 DAYS REPT 1 ITS) (1-AUG-2007)
PAV= 6001.4 PSIA WCT=0.347 GOR= 0.37 MSCF/STB WGR= 1.4350 STB/MSCF
1
***** 8
SIMULATE AT 212.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 7 1 AUG 2007 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 11 TIME= 243.00 DAYS ( +31.0 DAYS REPT 1 ITS) (1-SEP-2007)
PAV= 5928.3 PSIA WCT=0.343 GOR= 0.37 MSCF/STB WGR= 1.4104 STB/MSCF
```

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1
***** 9
SIMULATE AT 243.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 8 1 SEP 2007 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 12 TIME= 273.00 DAYS ( +30.0 DAYS REPT 1 ITS) (1-OCT-2007)
PAV= 5858.0 PSIA WCT=0.340 GOR= 0.37 MSCF/STB WGR= 1.3913 STB/MSCF
1
***** 10
SIMULATE AT 273.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 9 1 OCT 2007 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 13 TIME= 304.00 DAYS ( +31.0 DAYS REPT 1 ITS) (1-NOV-2007)
PAV= 5785.5 PSIA WCT=0.337 GOR= 0.37 MSCF/STB WGR= 1.3756 STB/MSCF
1
***** 11
SIMULATE AT 304.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 10 1 NOV 2007 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 14 TIME= 334.00 DAYS ( +30.0 DAYS REPT 1 ITS) (1-DEC-2007)
PAV= 5715.5 PSIA WCT=0.335 GOR= 0.37 MSCF/STB WGR= 1.3631 STB/MSCF
1
***** 12
SIMULATE AT 334.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 11 1 DEC 2007 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 15 TIME= 365.00 DAYS ( +31.0 DAYS REPT 1 ITS) (1-JAN-2008)
PAV= 5643.4 PSIA WCT=0.334 GOR= 0.37 MSCF/STB WGR= 1.3525 STB/MSCF
1
***** 13
SIMULATE AT 365.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 12 1 JAN 2008 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 16 TIME= 396.00 DAYS ( +31.0 DAYS REPT 1 ITS) (1-FEB-2008)
PAV= 5571.3 PSIA WCT=0.332 GOR= 0.37 MSCF/STB WGR= 1.3433 STB/MSCF
1
***** 14
SIMULATE AT 396.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 13 1 FEB 2008 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 17 TIME= 424.00 DAYS ( +28.0 DAYS REPT 1 ITS) (29-FEB-2008)
PAV= 5506.4 PSIA WCT=0.331 GOR= 0.37 MSCF/STB WGR= 1.3358 STB/MSCF
1
***** 15
SIMULATE AT 424.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
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REPORT 14 29 FEB 2008 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 18 TIME= 455.00 DAYS (+31.0 DAYS REPT 2 ITS) (31-MAR-2008)
PAV= 5434.5 PSIA WCT=0.330 GOR= 0.37 MSCF/STB WGR= 1.3283 STB/MSCF

1
***** 16

SIMULATE AT 455.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 15 31 MAR 2008 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 19 TIME= 485.00 DAYS (+30.0 DAYS REPT 2 ITS) (30-APR-2008)
PAV= 5365.0 PSIA WCT=0.328 GOR= 0.37 MSCF/STB WGR= 1.3214 STB/MSCF

1
***** 17

SIMULATE AT 485.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 16 30 APR 2008 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 20 TIME= 516.00 DAYS (+31.0 DAYS REPT 2 ITS) (31-MAY-2008)
PAV= 5293.3 PSIA WCT=0.327 GOR= 0.37 MSCF/STB WGR= 1.3147 STB/MSCF

1
***** 18

SIMULATE AT 516.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 17 31 MAY 2008 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 21 TIME= 546.00 DAYS (+30.0 DAYS REPT 2 ITS) (30-JUN-2008)
PAV= 5223.8 PSIA WCT=0.326 GOR= 0.37 MSCF/STB WGR= 1.3084 STB/MSCF

1
***** 19

SIMULATE AT 546.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 18 30 JUN 2008 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 22 TIME= 577.00 DAYS (+31.0 DAYS REPT 2 ITS) (31-JULY-2008)
PAV= 5152.1 PSIA WCT=0.325 GOR= 0.37 MSCF/STB WGR= 1.3020 STB/MSCF

1
***** 20

SIMULATE AT 577.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 19 31 JULY 2008 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 23 TIME= 608.00 DAYS (+31.0 DAYS REPT 2 ITS) (31-AUG-2008)
PAV= 5080.3 PSIA WCT=0.324 GOR= 0.37 MSCF/STB WGR= 1.2958 STB/MSCF

1
***** 21

SIMULATE AT 608.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 20 31 AUG 2008 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

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STEP 24 TIME= 638.00 DAYS (+30.0 DAYS REPT 2 ITS) (30-SEP-2008)
PAV= 5011.0 PSIA WCT=0.323 GOR= 0.37 MSCF/STB WGR= 1.2898 STB/MSCF
1
***** 22
SIMULATE AT 638.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 21 30 SEP 2008 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 25 TIME= 669.00 DAYS (+31.0 DAYS REPT 2 ITS) (31-OCT-2008)
PAV= 4939.3 PSIA WCT=0.322 GOR= 0.37 MSCF/STB WGR= 1.2837 STB/MSCF
1
***** 23
SIMULATE AT 669.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 22 31 OCT 2008 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 26 TIME= 699.00 DAYS (+30.0 DAYS REPT 2 ITS) (30-NOV-2008)
PAV= 4869.9 PSIA WCT=0.321 GOR= 0.37 MSCF/STB WGR= 1.2779 STB/MSCF
1
***** 24
SIMULATE AT 699.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 23 30 NOV 2008 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 27 TIME= 730.00 DAYS (+31.0 DAYS REPT 1 ITS) (31-DEC-2008)
PAV= 4798.4 PSIA WCT=0.320 GOR= 0.37 MSCF/STB WGR= 1.2720 STB/MSCF
59 READING WELSPecs
60 READING COMPDAT
61 READING WCONPROD
62 READING WCONINJE
63 READING TSTEP
1
***** 25
SIMULATE AT 730.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 24 31 DEC 2008 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

@--MESSAGE AT TIME 730.0 DAYS (31-DEC-2008):
@ *****
@ * WELL I1 HAS CHANGED TO *
@ * CONTROL BY BOTTOM HOLE PRESSURE *
@ * FROM TIME 730.00 DAYS *
@ *****

@--MESSAGE AT TIME 730.0 DAYS (31-DEC-2008):
@ *****
@ * WELL I2 HAS CHANGED TO *
@ * CONTROL BY BOTTOM HOLE PRESSURE *
@ * FROM TIME 730.00 DAYS *
@ *****

@--MESSAGE AT TIME 730.0 DAYS (31-DEC-2008):
@ *****
@ * WELL I3 HAS CHANGED TO *
@ * CONTROL BY BOTTOM HOLE PRESSURE *
@ * FROM TIME 730.00 DAYS *
@ *****

@--MESSAGE AT TIME 730.0 DAYS (31-DEC-2008):

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@ *****
@ * WELL I4 HAS CHANGED TO *
@ * CONTROL BY BOTTOM HOLE PRESSURE *
@ * FROM TIME 730.00 DAYS *
@ *****

STEP 28 TIME= 761.00 DAYS (+31.0 DAYS REPT 2 ITS) (31-JAN-2009)
PAV= 4774.8 PSIA WCT=0.321 GOR= 0.37 MSCF/STB WGR= 1.2759 STB/MSCF

1 ***** 26
SIMULATE AT 761.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 25 31 JAN 2009 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 29 TIME= 789.00 DAYS (+28.0 DAYS REPT 2 ITS) (28-FEB-2009)
PAV= 4753.2 PSIA WCT=0.324 GOR= 0.37 MSCF/STB WGR= 1.2926 STB/MSCF

1 ***** 27
SIMULATE AT 789.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 26 28 FEB 2009 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 30 TIME= 820.00 DAYS (+31.0 DAYS REPT 2 ITS) (31-MAR-2009)
PAV= 4730.5 PSIA WCT=0.330 GOR= 0.37 MSCF/STB WGR= 1.3310 STB/MSCF

1 ***** 28
SIMULATE AT 820.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 27 31 MAR 2009 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 31 TIME= 850.00 DAYS (+30.0 DAYS REPT 2 ITS) (30-APR-2009)
PAV= 4710.4 PSIA WCT=0.340 GOR= 0.37 MSCF/STB WGR= 1.3902 STB/MSCF

1 ***** 29
SIMULATE AT 850.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 28 30 APR 2009 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 32 TIME= 881.00 DAYS (+31.0 DAYS REPT 1 ITS) (31-MAY-2009)
PAV= 4691.7 PSIA WCT=0.353 GOR= 0.37 MSCF/STB WGR= 1.4763 STB/MSCF

1 ***** 30
SIMULATE AT 881.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 29 31 MAY 2009 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 33 TIME= 911.00 DAYS (+30.0 DAYS REPT 1 ITS) (30-JUN-2009)
PAV= 4675.0 PSIA WCT=0.370 GOR= 0.37 MSCF/STB WGR= 1.5854 STB/MSCF

1 ***** 31
SIMULATE AT 911.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 30 30 JUN 2009 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

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STEP 34 TIME= 942.00 DAYS ( +31.0 DAYS REPT 2 ITS) (31-JLY-2009)
PAV= 4658.9 PSIA WCT=0.390 GOR= 0.37 MSCF/STB WGR= 1.7263 STB/MSCF
1
***** 32
SIMULATE AT 942.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 31 31 JLY 2009 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 35 TIME= 973.00 DAYS ( +31.0 DAYS REPT 2 ITS) (31-AUG-2009)
PAV= 4643.6 PSIA WCT=0.412 GOR= 0.37 MSCF/STB WGR= 1.8942 STB/MSCF
1
***** 33
SIMULATE AT 973.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 32 31 AUG 2009 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 36 TIME= 1003.00 DAYS ( +30.0 DAYS REPT 2 ITS) (30-SEP-2009)
PAV= 4629.5 PSIA WCT=0.435 GOR= 0.37 MSCF/STB WGR= 2.0823 STB/MSCF
1
***** 34
SIMULATE AT 1003.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 33 30 SEP 2009 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 37 TIME= 1034.00 DAYS ( +31.0 DAYS REPT 2 ITS) (31-OCT-2009)
PAV= 4615.3 PSIA WCT=0.460 GOR= 0.37 MSCF/STB WGR= 2.3006 STB/MSCF
1
***** 35
SIMULATE AT 1034.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 34 31 OCT 2009 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 38 TIME= 1064.00 DAYS ( +30.0 DAYS REPT 2 ITS) (30-NOV-2009)
PAV= 4601.9 PSIA WCT=0.484 GOR= 0.37 MSCF/STB WGR= 2.5318 STB/MSCF
1
***** 36
SIMULATE AT 1064.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 35 30 NOV 2009 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 39 TIME= 1095.00 DAYS ( +31.0 DAYS REPT 2 ITS) (31-DEC-2009)
PAV= 4587.9 PSIA WCT=0.508 GOR= 0.37 MSCF/STB WGR= 2.7858 STB/MSCF
1
***** 37
SIMULATE AT 1095.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 36 31 DEC 2009 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 40 TIME= 1126.00 DAYS ( +31.0 DAYS REPT 2 ITS) (31-JAN-2010)
PAV= 4573.9 PSIA WCT=0.531 GOR= 0.37 MSCF/STB WGR= 3.0560 STB/MSCF
1
***** 38
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SIMULATE AT 1126.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 37 31 JAN 2010 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

@--MESSAGE AT TIME 1126.00 DAYS (31-JAN-2010):
@ *****
@ * WELL P HAS CHANGED TO *
@ * CONTROL BY BOTTOM HOLE PRESSURE *
@ * FROM TIME 1126.00 DAYS *
@ *****

STEP 41 TIME= 1154.00 DAYS (+28.0 DAYS REPT 2 ITS) (28-FEB-2010)
PAV= 4562.0 PSIA WCT=0.551 GOR= 0.37 MSCF/STB WGR= 3.3136 STB/MSCF

1 ***** 39

SIMULATE AT 1154.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 38 28 FEB 2010 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 42 TIME= 1185.00 DAYS (+31.0 DAYS REPT 2 ITS) (31-MAR-2010)
PAV= 4551.8 PSIA WCT=0.572 GOR= 0.37 MSCF/STB WGR= 3.6093 STB/MSCF

1 ***** 40

SIMULATE AT 1185.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 39 31 MAR 2010 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 43 TIME= 1215.00 DAYS (+30.0 DAYS REPT 1 ITS) (30-APR-2010)
PAV= 4543.9 PSIA WCT=0.591 GOR= 0.37 MSCF/STB WGR= 3.9030 STB/MSCF

1 ***** 41

SIMULATE AT 1215.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 40 30 APR 2010 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 44 TIME= 1246.00 DAYS (+31.0 DAYS REPT 2 ITS) (31-MAY-2010)
PAV= 4537.5 PSIA WCT=0.609 GOR= 0.37 MSCF/STB WGR= 4.2126 STB/MSCF

1 ***** 42

SIMULATE AT 1246.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 41 31 MAY 2010 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 45 TIME= 1276.00 DAYS (+30.0 DAYS REPT 2 ITS) (30-JUN-2010)
PAV= 4532.8 PSIA WCT=0.626 GOR= 0.37 MSCF/STB WGR= 4.5171 STB/MSCF

1 ***** 43

SIMULATE AT 1276.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 42 30 JUN 2010 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 46 TIME= 1307.00 DAYS (+31.0 DAYS REPT 1 ITS) (31-JULY-2010)
PAV= 4529.4 PSIA WCT=0.642 GOR= 0.37 MSCF/STB WGR= 4.8362 STB/MSCF

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1
***** 44
SIMULATE AT 1307.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 43 31 JULY 2010 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 47 TIME= 1338.00 DAYS ( +31.0 DAYS REPT 1 ITS) (31-AUG-2010)
PAV= 4527.2 PSIA WCT=0.656 GOR= 0.37 MSCF/STB WGR= 5.1564 STB/MSCF
1
***** 45
SIMULATE AT 1338.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 44 31 AUG 2010 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 48 TIME= 1368.00 DAYS ( +30.0 DAYS REPT 1 ITS) (30-SEP-2010)
PAV= 4525.9 PSIA WCT=0.669 GOR= 0.37 MSCF/STB WGR= 5.4693 STB/MSCF
1
***** 46
SIMULATE AT 1368.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 45 30 SEP 2010 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 49 TIME= 1399.00 DAYS ( +31.0 DAYS REPT 1 ITS) (31-OCT-2010)
PAV= 4525.3 PSIA WCT=0.682 GOR= 0.37 MSCF/STB WGR= 5.7893 STB/MSCF
1
***** 47
SIMULATE AT 1399.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 46 31 OCT 2010 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 50 TIME= 1429.00 DAYS ( +30.0 DAYS REPT 1 ITS) (30-NOV-2010)
PAV= 4525.4 PSIA WCT=0.693 GOR= 0.37 MSCF/STB WGR= 6.1058 STB/MSCF
1
***** 48
SIMULATE AT 1429.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 47 30 NOV 2010 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 51 TIME= 1460.00 DAYS ( +31.0 DAYS REPT 1 ITS) (31-DEC-2010)
PAV= 4525.9 PSIA WCT=0.704 GOR= 0.37 MSCF/STB WGR= 6.4399 STB/MSCF
1
***** 49
SIMULATE AT 1460.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 48 31 DEC 2010 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 52 TIME= 1491.00 DAYS ( +31.0 DAYS REPT 2 ITS) (31-JAN-2011)
PAV= 4526.7 PSIA WCT=0.714 GOR= 0.37 MSCF/STB WGR= 6.7592 STB/MSCF
1
***** 50
SIMULATE AT 1491.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
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REPORT 49 31 JAN 2011 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 53 TIME= 1519.00 DAYS (+28.0 DAYS REPT 1 ITS) (28-FEB-2011)
PAV= 4527.3 PSIA WCT=0.723 GOR= 0.37 MSCF/STB WGR= 7.0554 STB/MSCF

1 ***** 51

SIMULATE AT 1519.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 50 28 FEB 2011 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 54 TIME= 1550.00 DAYS (+31.0 DAYS REPT 1 ITS) (31-MAR-2011)
PAV= 4528.2 PSIA WCT=0.732 GOR= 0.37 MSCF/STB WGR= 7.3974 STB/MSCF

1 ***** 52

SIMULATE AT 1550.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 51 31 MAR 2011 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 55 TIME= 1580.00 DAYS (+30.0 DAYS REPT 1 ITS) (30-APR-2011)
PAV= 4529.0 PSIA WCT=0.741 GOR= 0.37 MSCF/STB WGR= 7.7373 STB/MSCF

1 ***** 53

SIMULATE AT 1580.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 52 30 APR 2011 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 56 TIME= 1611.00 DAYS (+31.0 DAYS REPT 1 ITS) (31-MAY-2011)
PAV= 4529.8 PSIA WCT=0.750 GOR= 0.37 MSCF/STB WGR= 8.0962 STB/MSCF

1 ***** 54

SIMULATE AT 1611.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 53 31 MAY 2011 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 57 TIME= 1641.00 DAYS (+30.0 DAYS REPT 1 ITS) (30-JUN-2011)
PAV= 4530.6 PSIA WCT=0.758 GOR= 0.37 MSCF/STB WGR= 8.4506 STB/MSCF

1 ***** 55

SIMULATE AT 1641.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 54 30 JUN 2011 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 58 TIME= 1672.00 DAYS (+31.0 DAYS REPT 1 ITS) (31-JULY-2011)
PAV= 4531.4 PSIA WCT=0.766 GOR= 0.37 MSCF/STB WGR= 8.8229 STB/MSCF

1 ***** 56

SIMULATE AT 1672.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 55 31 JULY 2011 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

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STEP 59 TIME= 1703.00 DAYS (+31.0 DAYS REPT 1 ITS) (31-AUG-2011)
PAV= 4532.2 PSIA WCT=0.773 GOR= 0.37 MSCF/STB WGR= 9.2000 STB/MSCF

1
***** 57
SIMULATE AT 1703.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 56 31 AUG 2011 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 60 TIME= 1733.00 DAYS (+30.0 DAYS REPT 1 ITS) (30-SEP-2011)
PAV= 4533.0 PSIA WCT=0.780 GOR= 0.37 MSCF/STB WGR= 9.5688 STB/MSCF

1
***** 58
SIMULATE AT 1733.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 57 30 SEP 2011 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 61 TIME= 1764.00 DAYS (+31.0 DAYS REPT 1 ITS) (31-OCT-2011)
PAV= 4533.8 PSIA WCT=0.786 GOR= 0.37 MSCF/STB WGR= 9.9527 STB/MSCF

1
***** 59
SIMULATE AT 1764.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 58 31 OCT 2011 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 62 TIME= 1794.00 DAYS (+30.0 DAYS REPT 1 ITS) (30-NOV-2011)
PAV= 4534.5 PSIA WCT=0.793 GOR= 0.37 MSCF/STB WGR= 10.3249 STB/MSCF

1
***** 60
SIMULATE AT 1794.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 59 30 NOV 2011 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 63 TIME= 1825.00 DAYS (+31.0 DAYS REPT 1 ITS) (31-DEC-2011)
PAV= 4535.2 PSIA WCT=0.798 GOR= 0.37 MSCF/STB WGR= 10.7101 STB/MSCF

1
***** 61
SIMULATE AT 1825.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 60 31 DEC 2011 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 64 TIME= 1856.00 DAYS (+31.0 DAYS REPT 1 ITS) (31-JAN-2012)
PAV= 4535.9 PSIA WCT=0.804 GOR= 0.37 MSCF/STB WGR= 11.0924 STB/MSCF

1
***** 62
SIMULATE AT 1856.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 61 31 JAN 2012 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 65 TIME= 1884.00 DAYS (+28.0 DAYS REPT 1 ITS) (28-FEB-2012)
PAV= 4536.6 PSIA WCT=0.809 GOR= 0.37 MSCF/STB WGR= 11.4350 STB/MSCF

1
***** 63

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SIMULATE AT 1884.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 62 28 FEB 2012 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 66 TIME= 1915.00 DAYS (+31.0 DAYS REPT 1 ITS) (30-MAR-2012)
PAV= 4537.2 PSIA WCT=0.814 GOR= 0.37 MSCF/STB WGR= 11.8001 STB/MSCF

1
***** 64
SIMULATE AT 1915.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 63 30 MAR 2012 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 67 TIME= 1945.00 DAYS (+30.0 DAYS REPT 2 ITS) (29-APR-2012)
PAV= 4537.9 PSIA WCT=0.818 GOR= 0.37 MSCF/STB WGR= 12.1542 STB/MSCF

1
***** 65
SIMULATE AT 1945.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 64 29 APR 2012 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 68 TIME= 1976.00 DAYS (+31.0 DAYS REPT 1 ITS) (30-MAY-2012)
PAV= 4538.5 PSIA WCT=0.822 GOR= 0.37 MSCF/STB WGR= 12.5214 STB/MSCF

1
***** 66
SIMULATE AT 1976.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 65 30 MAY 2012 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 69 TIME= 2006.00 DAYS (+30.0 DAYS REPT 1 ITS) (29-JUN-2012)
PAV= 4539.1 PSIA WCT=0.827 GOR= 0.37 MSCF/STB WGR= 12.8789 STB/MSCF

1
***** 67
SIMULATE AT 2006.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 66 29 JUN 2012 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 70 TIME= 2037.00 DAYS (+31.0 DAYS REPT 1 ITS) (30-JULY-2012)
PAV= 4539.8 PSIA WCT=0.831 GOR= 0.37 MSCF/STB WGR= 13.2488 STB/MSCF

1
***** 68
SIMULATE AT 2037.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 67 30 JULY 2012 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 71 TIME= 2068.00 DAYS (+31.0 DAYS REPT 1 ITS) (30-AUG-2012)
PAV= 4540.4 PSIA WCT=0.834 GOR= 0.37 MSCF/STB WGR= 13.6097 STB/MSCF

1
***** 69
SIMULATE AT 2068.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 68 30 AUG 2012 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

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*****
STEP 72 TIME= 2098.00 DAYS ( +30.0 DAYS REPT 1 ITS) (29-SEP-2012)
PAV= 4540.9 PSIA WCT=0.838 GOR= 0.37 MSCF/STB WGR= 13.9626 STB/MSCF
1
***** 70
SIMULATE AT 2098.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 69 29 SEP 2012 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****
STEP 73 TIME= 2129.00 DAYS ( +31.0 DAYS REPT 1 ITS) (30-OCT-2012)
PAV= 4541.5 PSIA WCT=0.841 GOR= 0.37 MSCF/STB WGR= 14.3318 STB/MSCF
1
***** 71
SIMULATE AT 2129.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 70 30 OCT 2012 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****
STEP 74 TIME= 2159.00 DAYS ( +30.0 DAYS REPT 1 ITS) (29-NOV-2012)
PAV= 4542.0 PSIA WCT=0.845 GOR= 0.37 MSCF/STB WGR= 14.6936 STB/MSCF
1
***** 72
SIMULATE AT 2159.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 71 29 NOV 2012 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****
STEP 75 TIME= 2190.00 DAYS ( +31.0 DAYS REPT 1 ITS) (30-DEC-2012)
PAV= 4542.5 PSIA WCT=0.848 GOR= 0.37 MSCF/STB WGR= 15.0720 STB/MSCF
1
***** 73
SIMULATE AT 2190.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 72 30 DEC 2012 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****
STEP 76 TIME= 2221.00 DAYS ( +31.0 DAYS REPT 1 ITS) (30-JAN-2013)
PAV= 4543.0 PSIA WCT=0.851 GOR= 0.37 MSCF/STB WGR= 15.4546 STB/MSCF
1
***** 74
SIMULATE AT 2221.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 73 30 JAN 2013 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****
STEP 77 TIME= 2249.00 DAYS ( +28.0 DAYS REPT 2 ITS) (27-FEB-2013)
PAV= 4543.5 PSIA WCT=0.854 GOR= 0.37 MSCF/STB WGR= 15.8039 STB/MSCF
1
***** 75
SIMULATE AT 2249.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 74 27 FEB 2013 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****
STEP 78 TIME= 2280.00 DAYS ( +31.0 DAYS REPT 1 ITS) (30-MAR-2013)
PAV= 4544.0 PSIA WCT=0.857 GOR= 0.37 MSCF/STB WGR= 16.1936 STB/MSCF
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1
***** 76
SIMULATE AT 2280.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 75 30 MAR 2013 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 79 TIME= 2310.00 DAYS ( +30.0 DAYS REPT 1 ITS) (29-APR-2013)
PAV= 4544.5 PSIA WCT=0.860 GOR= 0.37 MSCF/STB WGR= 16.5741 STB/MSCF
1
***** 77
SIMULATE AT 2310.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 76 29 APR 2013 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 80 TIME= 2341.00 DAYS ( +31.0 DAYS REPT 1 ITS) (30-MAY-2013)
PAV= 4545.0 PSIA WCT=0.862 GOR= 0.37 MSCF/STB WGR= 16.9518 STB/MSCF
1
***** 78
SIMULATE AT 2341.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 77 30 MAY 2013 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 81 TIME= 2371.00 DAYS ( +30.0 DAYS REPT 1 ITS) (29-JUN-2013)
PAV= 4545.5 PSIA WCT=0.865 GOR= 0.37 MSCF/STB WGR= 17.3223 STB/MSCF
1
***** 79
SIMULATE AT 2371.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 78 29 JUN 2013 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 82 TIME= 2402.00 DAYS ( +31.0 DAYS REPT 1 ITS) (30-JULY-2013)
PAV= 4546.0 PSIA WCT=0.867 GOR= 0.37 MSCF/STB WGR= 17.6921 STB/MSCF
1
***** 80
SIMULATE AT 2402.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 79 30 JULY 2013 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 83 TIME= 2433.00 DAYS ( +31.0 DAYS REPT 1 ITS) (30-AUG-2013)
PAV= 4546.5 PSIA WCT=0.870 GOR= 0.37 MSCF/STB WGR= 18.0676 STB/MSCF
1
***** 81
SIMULATE AT 2433.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 80 30 AUG 2013 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****

STEP 84 TIME= 2463.00 DAYS ( +30.0 DAYS REPT 1 ITS) (29-SEP-2013)
PAV= 4547.0 PSIA WCT=0.872 GOR= 0.37 MSCF/STB WGR= 18.4369 STB/MSCF
1
***** 82
SIMULATE AT 2463.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
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REPORT 81 29 SEP 2013 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 85 TIME= 2494.00 DAYS (+31.0 DAYS REPT 1 ITS) (30-OCT-2013)
PAV= 4547.4 PSIA WCT=0.874 GOR= 0.37 MSCF/STB WGR= 18.8238 STB/MSCF

1 ***** 83

SIMULATE AT 2494.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 82 30 OCT 2013 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 86 TIME= 2524.00 DAYS (+30.0 DAYS REPT 1 ITS) (29-NOV-2013)
PAV= 4547.9 PSIA WCT=0.877 GOR= 0.37 MSCF/STB WGR= 19.2025 STB/MSCF

1 ***** 84

SIMULATE AT 2524.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 83 29 NOV 2013 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 87 TIME= 2555.00 DAYS (+31.0 DAYS REPT 1 ITS) (30-DEC-2013)
PAV= 4548.3 PSIA WCT=0.879 GOR= 0.37 MSCF/STB WGR= 19.5969 STB/MSCF

1 ***** 85

SIMULATE AT 2555.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 84 30 DEC 2013 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 88 TIME= 2586.00 DAYS (+31.0 DAYS REPT 2 ITS) (30-JAN-2014)
PAV= 4548.7 PSIA WCT=0.881 GOR= 0.37 MSCF/STB WGR= 19.9479 STB/MSCF

1 ***** 86

SIMULATE AT 2586.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 85 30 JAN 2014 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 89 TIME= 2614.00 DAYS (+28.0 DAYS REPT 1 ITS) (27-FEB-2014)
PAV= 4548.9 PSIA WCT=0.882 GOR= 0.37 MSCF/STB WGR= 20.2868 STB/MSCF

1 ***** 87

SIMULATE AT 2614.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 86 27 FEB 2014 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 90 TIME= 2645.00 DAYS (+31.0 DAYS REPT 1 ITS) (30-MAR-2014)
PAV= 4549.1 PSIA WCT=0.884 GOR= 0.37 MSCF/STB WGR= 20.6753 STB/MSCF

1 ***** 88

SIMULATE AT 2645.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 87 30 MAR 2014 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

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STEP 91 TIME= 2675.00 DAYS ( +30.0 DAYS REPT 1 ITS) (29-APR-2014)
PAV= 4549.2 PSIA WCT=0.886 GOR= 0.37 MSCF/STB WGR= 21.0582 STB/MSCF
1
***** 89
SIMULATE AT 2675.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 88 29 APR 2014 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007
*****

STEP 92 TIME= 2706.00 DAYS ( +31.0 DAYS REPT 1 ITS) (30-MAY-2014)
PAV= 4549.2 PSIA WCT=0.888 GOR= 0.37 MSCF/STB WGR= 21.4577 STB/MSCF
1
***** 90
SIMULATE AT 2706.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 89 30 MAY 2014 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007
*****

STEP 93 TIME= 2736.00 DAYS ( +30.0 DAYS REPT 1 ITS) (29-JUN-2014)
PAV= 4549.2 PSIA WCT=0.890 GOR= 0.37 MSCF/STB WGR= 21.8470 STB/MSCF
1
***** 91
SIMULATE AT 2736.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 90 29 JUN 2014 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007
*****

STEP 94 TIME= 2767.00 DAYS ( +31.0 DAYS REPT 1 ITS) (30-JULY-2014)
PAV= 4549.1 PSIA WCT=0.892 GOR= 0.37 MSCF/STB WGR= 22.2509 STB/MSCF
1
***** 92
SIMULATE AT 2767.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 91 30 JULY 2014 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007
*****

STEP 95 TIME= 2798.00 DAYS ( +31.0 DAYS REPT 1 ITS) (30-AUG-2014)
PAV= 4549.0 PSIA WCT=0.893 GOR= 0.37 MSCF/STB WGR= 22.6562 STB/MSCF
1
***** 93
SIMULATE AT 2798.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 92 30 AUG 2014 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007
*****

STEP 96 TIME= 2828.00 DAYS ( +30.0 DAYS REPT 1 ITS) (29-SEP-2014)
PAV= 4548.9 PSIA WCT=0.895 GOR= 0.37 MSCF/STB WGR= 23.0475 STB/MSCF
1
***** 94
SIMULATE AT 2828.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 93 29 SEP 2014 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007
*****

STEP 97 TIME= 2859.00 DAYS ( +31.0 DAYS REPT 1 ITS) (30-OCT-2014)
PAV= 4548.8 PSIA WCT=0.897 GOR= 0.37 MSCF/STB WGR= 23.4503 STB/MSCF
1
***** 95
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SIMULATE AT 2859.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 94 30 OCT 2014 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 98 TIME= 2889.00 DAYS (+30.0 DAYS REPT 1 ITS) (29-NOV-2014)
PAV= 4548.6 PSIA WCT=0.898 GOR= 0.37 MSCF/STB WGR= 23.8269 STB/MSCF

1 ***** 96

SIMULATE AT 2889.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 95 29 NOV 2014 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 99 TIME= 2920.00 DAYS (+31.0 DAYS REPT 1 ITS) (30-DEC-2014)
PAV= 4548.4 PSIA WCT=0.900 GOR= 0.37 MSCF/STB WGR= 24.2133 STB/MSCF

1 ***** 97

SIMULATE AT 2920.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 96 30 DEC 2014 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 100 TIME= 2951.00 DAYS (+31.0 DAYS REPT 1 ITS) (30-JAN-2015)
PAV= 4548.3 PSIA WCT=0.901 GOR= 0.37 MSCF/STB WGR= 24.5991 STB/MSCF

1 ***** 98

SIMULATE AT 2951.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 97 30 JAN 2015 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 101 TIME= 2979.00 DAYS (+28.0 DAYS REPT 1 ITS) (27-FEB-2015)
PAV= 4548.1 PSIA WCT=0.902 GOR= 0.37 MSCF/STB WGR= 24.9479 STB/MSCF

1 ***** 99

SIMULATE AT 2979.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 98 27 FEB 2015 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 102 TIME= 3010.00 DAYS (+31.0 DAYS REPT 1 ITS) (30-MAR-2015)
PAV= 4547.9 PSIA WCT=0.904 GOR= 0.37 MSCF/STB WGR= 25.3340 STB/MSCF

1 ***** 100

SIMULATE AT 3010.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 99 30 MAR 2015 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 103 TIME= 3040.00 DAYS (+30.0 DAYS REPT 1 ITS) (29-APR-2015)
PAV= 4547.7 PSIA WCT=0.905 GOR= 0.37 MSCF/STB WGR= 25.7084 STB/MSCF

1 ***** 101

SIMULATE AT 3040.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 100 29 APR 2015 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

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*****
STEP 104 TIME= 3071.00 DAYS (+31.0 DAYS REPT 1 ITS) (30-MAY-2015)
PAV= 4547.5 PSIA WCT=0.906 GOR= 0.37 MSCF/STB WGR= 26.0951 STB/MSCF
SIMULATE AT 3071.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 101 30 MAY 2015 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007
*****
STEP 105 TIME= 3101.00 DAYS (+30.0 DAYS REPT 1 ITS) (29-JUN-2015)
PAV= 4547.4 PSIA WCT=0.907 GOR= 0.37 MSCF/STB WGR= 26.4693 STB/MSCF
SIMULATE AT 3101.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 102 29 JUN 2015 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007
*****
STEP 106 TIME= 3132.00 DAYS (+31.0 DAYS REPT 1 ITS) (30-JULY-2015)
PAV= 4547.2 PSIA WCT=0.909 GOR= 0.37 MSCF/STB WGR= 26.8546 STB/MSCF
SIMULATE AT 3132.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 103 30 JULY 2015 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007
*****
STEP 107 TIME= 3163.00 DAYS (+31.0 DAYS REPT 1 ITS) (30-AUG-2015)
PAV= 4547.0 PSIA WCT=0.910 GOR= 0.37 MSCF/STB WGR= 27.2386 STB/MSCF
SIMULATE AT 3163.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 104 30 AUG 2015 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007
*****
STEP 108 TIME= 3193.00 DAYS (+30.0 DAYS REPT 1 ITS) (29-SEP-2015)
PAV= 4546.8 PSIA WCT=0.911 GOR= 0.37 MSCF/STB WGR= 27.6079 STB/MSCF
SIMULATE AT 3193.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 105 29 SEP 2015 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007
*****
STEP 109 TIME= 3224.00 DAYS (+31.0 DAYS REPT 1 ITS) (30-OCT-2015)
PAV= 4546.7 PSIA WCT=0.912 GOR= 0.37 MSCF/STB WGR= 27.9864 STB/MSCF
SIMULATE AT 3224.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 106 30 OCT 2015 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007
*****
STEP 110 TIME= 3254.00 DAYS (+30.0 DAYS REPT 1 ITS) (29-NOV-2015)
PAV= 4546.5 PSIA WCT=0.913 GOR= 0.37 MSCF/STB WGR= 28.3501 STB/MSCF
*****

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*****
STEP 104 TIME= 3071.00 DAYS ( +31.0 DAYS REPT 1 ITS) (30-MAY-2015)
PAV= 4547.5 PSIA WCT=0.906 GOR= 0.37 MSCF/STB WGR= 26.0951 STB/MSCF
1
***** 102
SIMULATE AT 3071.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 101 30 MAY 2015 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****
STEP 105 TIME= 3101.00 DAYS ( +30.0 DAYS REPT 1 ITS) (29-JUN-2015)
PAV= 4547.4 PSIA WCT=0.907 GOR= 0.37 MSCF/STB WGR= 26.4693 STB/MSCF
1
***** 103
SIMULATE AT 3101.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 102 29 JUN 2015 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****
STEP 106 TIME= 3132.00 DAYS ( +31.0 DAYS REPT 1 ITS) (30-JULY-2015)
PAV= 4547.2 PSIA WCT=0.909 GOR= 0.37 MSCF/STB WGR= 26.8546 STB/MSCF
1
***** 104
SIMULATE AT 3132.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 103 30 JULY 2015 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****
STEP 107 TIME= 3163.00 DAYS ( +31.0 DAYS REPT 1 ITS) (30-AUG-2015)
PAV= 4547.0 PSIA WCT=0.910 GOR= 0.37 MSCF/STB WGR= 27.2386 STB/MSCF
1
***** 105
SIMULATE AT 3163.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 104 30 AUG 2015 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****
STEP 108 TIME= 3193.00 DAYS ( +30.0 DAYS REPT 1 ITS) (29-SEP-2015)
PAV= 4546.8 PSIA WCT=0.911 GOR= 0.37 MSCF/STB WGR= 27.6079 STB/MSCF
1
***** 106
SIMULATE AT 3193.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 105 29 SEP 2015 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****
STEP 109 TIME= 3224.00 DAYS ( +31.0 DAYS REPT 1 ITS) (30-OCT-2015)
PAV= 4546.7 PSIA WCT=0.912 GOR= 0.37 MSCF/STB WGR= 27.9864 STB/MSCF
1
***** 107
SIMULATE AT 3224.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 106 30 OCT 2015 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

*****
STEP 110 TIME= 3254.00 DAYS ( +30.0 DAYS REPT 1 ITS) (29-NOV-2015)
PAV= 4546.5 PSIA WCT=0.913 GOR= 0.37 MSCF/STB WGR= 28.3501 STB/MSCF
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1

***** 108

SIMULATE AT 3254.00 DAYS *INITIAL
* ECLIPSE VERSION 2005a
REPORT 107 29 NOV 2015 *WIN32 RUN
* RUN AT 14:30 ON 01 MAY 2007

STEP 111 TIME= 3285.00 DAYS (+31.0 DAYS REPT 1 ITS) (30-DEC-2015)
PAV= 4546.3 PSIA WCT=0.914 GOR= 0.37 MSCF/STB WGR= 28.7228 STB/MSCF
64 READING END

Error summary

Comments	1
Warnings	3
Problems	0
Errors	0
Bugs	0