

Name:	
Enrolment No:	

UNIVERSITY OF PETROLEUM AND ENERGY STUDIES
End Semester Examination, December 2018

Course: Finite Volume Methods for conservation laws (ASEG7021) Semester: I
Programme: M. Tech CFD
Time: 03 hrs. Max. Marks: 100
Instructions: Make use of sketch/plots to elaborate your answer. All sections are compulsory.

SECTION A

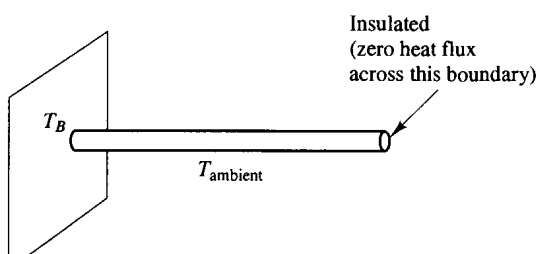
S. No.		Marks	CO
Q 1.	Differentiate between Lagrangian and Eulerian descriptions. Give suitable example clearly stating advantages and disadvantages for each description.	[04]	CO1
Q 2.	Classify the steady two-dimensional velocity potential equation: $(1 - M^2) \phi_{xx} + \phi_{yy} = 0$ where M is mach number. Explain the physical meaning of various classifications based on M .	[04]	CO2
Q 3.	Explain the algorithm of the Jacobi Iteration method applied to a parabolic partial differential equation.	[04]	CO2
Q 4.	Define the following terms: a) Diffusion number b) Approximate factorization	[04]	CO1
Q 5.	What is the stability requirement of an explicit finite difference equation produced from the model equation $\frac{\partial u}{\partial t} = \alpha \left[\frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial x^2} \right]$.	[04]	CO3

SECTION B

Q 6.	Explain the basic methodology of Finite Difference Method. Derive the discretization equation with the help of Taylors series for the following methods, <ul style="list-style-type: none"> • Forward Difference • Backward Difference • Central Difference State the accuracy and stability criteria for each method.	[10]	CO1
Q 7.	Derive the explicit MacCormack time marching algorithm for the solution of	[10]	CO2

	transient Euler equations in 2-dimensions		
Q 8.	Define the UPWIND interpolation scheme for the evaluation of fluxes at face centre using the nodal values on a structured finite volume grid. Find an expression for the artificial diffusivity introduced by this scheme.	[10]	CO3
Q 9.	Describe the underlying concept of the following terminologies: a) Consistency b) Stability c) Convergence d) Conservative property	[10]	CO3

SECTION-C

Q 10.	<p>Shown in Figure below is a cylindrical fin with uniform cross-sectional area A. The base is at a temperature of 100 °C (T_B) and the end is insulated. The fin is exposed to an ambient temperature of 20 °C. One-dimensional heat transfer in this situation is governed by</p> $\frac{d}{dx} \left(kA \frac{dT}{dx} \right) - hP(T - T_\infty) = 0$ <p>where h is the convective heat transfer coefficient, P the perimeter, k the thermal conductivity of the material and T_∞ the ambient temperature.</p>  <p>Calculate the temperature distribution along the fin and compare the results with the analytical solution given by</p> $\frac{T - T_\infty}{T_B - T_\infty} = \frac{\cosh[n(L - x)]}{\cosh(nL)}$ <p>where $n^2 = hP/(kA)$, L is the length of the fin and x the distance along the fin. Data: L = 1 m, $hP/(kA) = 25 \text{ m}^{-2}$ (note kA is constant). Solve for 5 and 10 nodes. Compare the result.</p>	[20]	CO4
Q 11.	Consider the model equation:		

$$a \frac{\partial u}{\partial x} = \nu \frac{\partial^2 u}{\partial y^2}$$

- (a) Write an explicit formulation using a first-order forward differencing in x and a second-order central differencing in y .
- (b) Use von Neumann stability analysis to determine the stability requirement of the scheme.

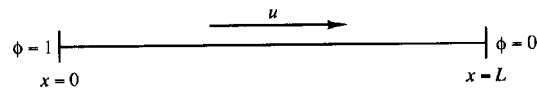
OR

A property ϕ is transported by means of convection and diffusion through the one-dimensional domain sketched in figure below. The governing equation below;

$$\frac{d}{dx}(\rho u \phi) = \frac{d}{dx} \left(\tau \frac{d\phi}{dx} \right)$$

boundary conditions are $\phi_0 = 1$ at $x = 0$ and $\phi_L = 0$ at $x = L$. Using five equally spaced cells (for first two cases) and the central differencing scheme for convection and diffusion calculate the distribution of ϕ as a function of x for cases:

- (i) Case 1: $u = 0.1$ m/s, using 5 cells
(ii) Case 2: $u = 2.5$ m/s, using 5 cells
(iii) Case 3: $u = 2.5$ using 10 cells



and compare the results with the analytical solution given below. The following data apply: length $L = 1.0$ m, $\rho = 1.0$ kg/m³, $\Gamma = 0.1$ kg/m/s.

$$\frac{\phi - \phi_0}{\phi_L - \phi_0} = \frac{\exp(\rho u x / \Gamma) - 1}{\exp(\rho u L / \Gamma) - 1}$$

[20]

CO4

Name:

Enrolment No:



UNIVERSITY OF PETROLEUM AND ENERGY STUDIES

End Semester Examination, December 2018

Course: Finite Volume Method for conservation laws (ASEG7021)

Semester: I

Programme: M. Tech CFD

Time: 03 hrs.

Max. Marks: 100

Instructions: Make use of sketch/plots to elaborate your answer. All sections are compulsory.

SECTION A

S. No.		Marks	CO
Q 1.	Under what conditions, the Navier-Stokes equation will become, <ul style="list-style-type: none">• Elliptic• Parabolic• Hyperbolic	[04]	CO2
Q 2.	Differentiate between explicit and implicit methods for converting partial differential equations into finite difference equations.	[04]	CO1
Q 3.	Find a forward difference approximation of $O(\Delta x)$ for $\frac{\partial^4 f}{\partial x^4}$	[04]	CO2
Q 4.	What do you mean by initial and boundary conditions? Define various types of boundary conditions which are usually encountered in CFD problems.	[04]	CO1
Q 5.	What is the importance of CFL condition? Relate it to the analysis of stability?	[04]	CO3

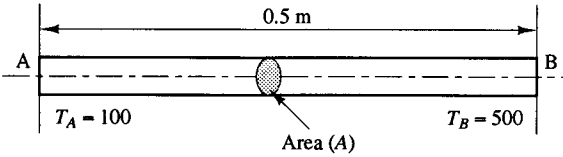
SECTION B

Q 6.	Explain with proper example how a pentadiagonal coefficient matrix can be reduced to two sets of tridiagonal coefficient matrix to be solved in sequence.	[10]	CO1
Q 7.	Determine an approximate backward difference representation for $\frac{\partial^3 f}{\partial x^3}$ which is of order (Δx) , given evenly spaced grid points by means of: <ul style="list-style-type: none">(a) Taylor series expansions.(b) A backward difference recurrence formulae(c) A third-degree polynomial passing through four points.	[10]	CO2
Q 8.	Given the function $f(x) = \frac{1}{4}x^2$, compute the first derivative of f at $x=2$ using forward and backward differencing of order (Δx) . Compare the results with a central differencing of $O(\Delta x)^2$ and the exact analytical value. Repeat the computations for a step size of 0.4.	[10]	CO3

Q 9.	<p>Explain the various methods for the approximation of surface integrals over a 2 - dimensional control volume.</p> <p style="text-align: center;">OR</p> <p>Derive the explicit Mac-Cormack time marching algorithm for the solution of transient Euler equations in 2-Dimensions.</p>	[10]	CO3
------	---	------	-----

SECTION C

Q 10.	<p>Given the following data, compute $f'(5)$, $f'(7)$ and $f'(9)$. Use finite difference of order (Δx). Compare the results to the values obtained by finite differencing of order $(\Delta x)^2$.</p> <table border="1" style="margin: auto;"> <tr> <td style="text-align: center;">x</td> <td style="text-align: center;">5</td> <td style="text-align: center;">6</td> <td style="text-align: center;">7</td> <td style="text-align: center;">8</td> <td style="text-align: center;">9</td> </tr> <tr> <td style="text-align: center;">$f(x)$</td> <td style="text-align: center;">25</td> <td style="text-align: center;">36</td> <td style="text-align: center;">49</td> <td style="text-align: center;">64</td> <td style="text-align: center;">81</td> </tr> </table>	x	5	6	7	8	9	$f(x)$	25	36	49	64	81	[20]	CO4
x	5	6	7	8	9										
$f(x)$	25	36	49	64	81										

Q 11.	<p>Consider the problem of source-free heat conduction in an insulated rod whose ends are maintained at constant temperatures of 100 °C and 500 °C respectively. The one-dimensional problem sketched in Figure below, is governed by</p> $\frac{d}{dx} \left(k \frac{dT}{dx} \right) = 0$ <p>Calculate the steady state temperature distribution in the rod. Thermal conductivity k equals 1000 W/m/K, cross-sectional area A is $10 \times 10^{-3} \text{ m}^2$. Use at least 5 control volumes with appropriate interpolation scheme.</p> <div style="text-align: center;">  </div>	[20]	CO4
-------	--	------	-----